

A. Class AB Analysis

- 1) Consider the Class AB current booster in Fig. 1. The input voltage is a $1V_{PP}$ sine wave at 2 kHz, the minimum load impedance is $R_L = 50 \text{ ohm}$. The op amp output swing is shown in the plot below. Assume “quick” analysis parameters for all components (i.e. diodes have $V_F = 0.7V$, transistors have $|V_{BE,ON}| = 0.7V$, $|V_{CE,SAT}| = 0V$, and $\beta = 100$).
- Compute the maximum load voltage and current (e.g. assume the entire circuit works properly). Hint: You know V_{IN} , and recall that an inverting amplifier has a gain $G = -R2/R1$.
 - We already have R_{B1} and R_{B2} . You must choose between $V_{CC} = 6, 9, 12, \text{ or } 15V$. Hint #1: What is the min V_{CC} needed to provide enough base current to Q1 when V_{LOAD} is maximum? Hint #2: Assume the 1 Mohm resistor current is so tiny it can be ignored. Hint #3: $V_{CC} > 8.3V$.
 - Using Fig. 1b, show the op amp can produce the necessary max V_O and I_O . Hint: Max I_O is $\approx 10 \text{ mA}$.

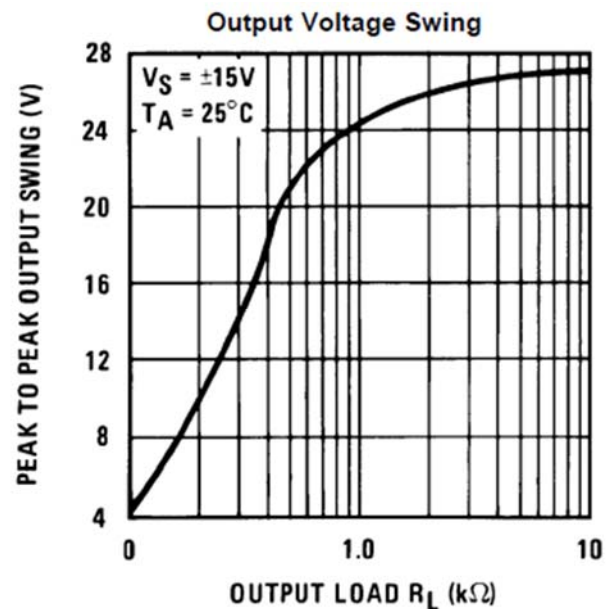
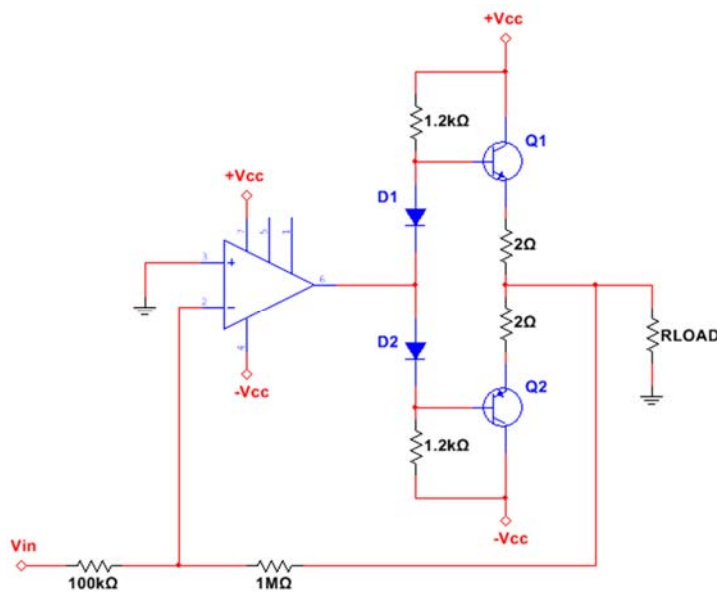


Fig. 1: (Left) Op amp with Class AB output stage. (Right) Op amp max output swing.

B. Class AB Design

- 2) Design an audio amplifier based on an op amp and Class AB stage (see Fig. 2). The design requirements are the following:
- Drive up to 400 mW (but not more) into a 32 ohm load.
 - The input signal is a sine wave with a maximum amplitude of $1V_{PP}$.
 - The input impedance must be $R_{IN} \geq 10 \text{ kohm}$.

- The low frequency cut-off is < 200 Hz (see part (g)).

The design constraints are the following:

- Q1 must be a 2N3904 or 2N4401. NOTE: The pnp versions are the 2N3906 and 2N4403.
- V_{CC} must be 4.5, 6, 9, or 12V.
- Use an LM741 op amp and 1N914 diodes (see website).
- All resistors are standard 5% tolerance.
- C_{OUT} must be 1, 10, 47, 100, or 470 μ F.

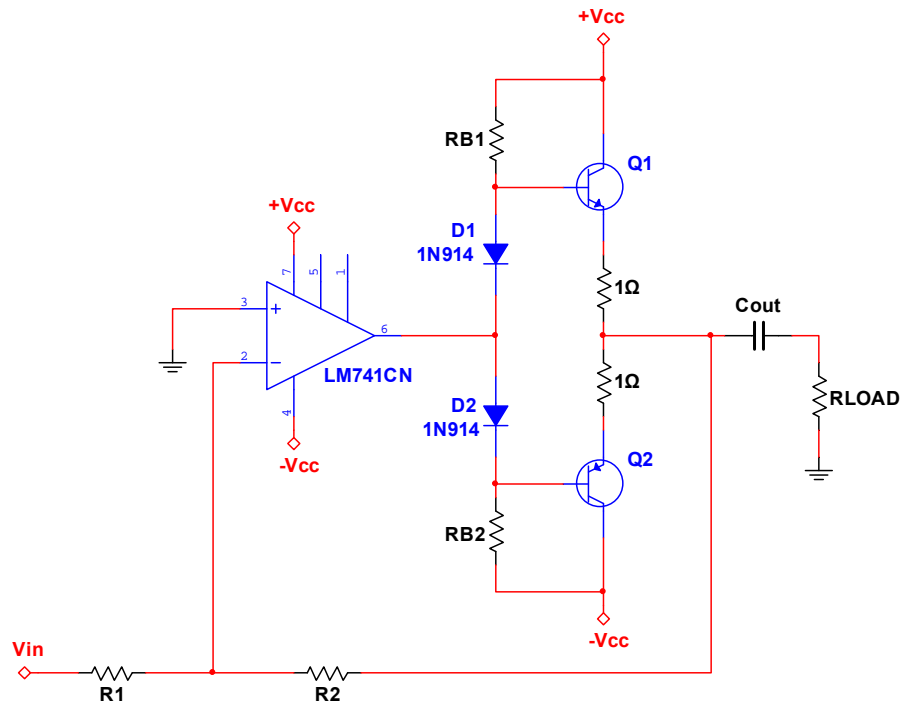


Fig. 2: Inverting amplifier with Class AB output stage. Remember that $G = -R2/R1$ for an inverting amplifier!

- Compute the max load voltage and current. Hint: Around 5.1V and 160 mA.
- Perform a “quick” analysis to find the minimum V_{CC} and then choose a V_{CC} (this may need to be changed later). Hint #1: As always, first assume C_{OUT} acts like a perfect short circuit (we’ll choose a proper value later). Hint #2: $V_{CC} > 7V$.
- Choose Q1 and Q2. Show all work! Hint #1: Assume “quick” analysis parameters when computing power dissipation in Q1! Hint #2: As always, you can ignore $R2$ current since it is usually much smaller than the load current. Hint #3: The 2N4401 should work. If you need a heat sink, then you MUST compute the necessary θ_{SA} .
- Choose R_{B1} and R_{B2} . Pick standard 5% values. Hint: Around 1 kohm.
- Show that the op amp can provide the required output voltage and current. **If it does not, then you must increase V_{CC} to a higher value and repeat part (c) and (d).**
- Choose $R1$ and $R2$. Remember that $G = -R2/R1$ and $R_{IN} = R1$ for an inverting amplifier. Keep in mind that your Class AB stage assumed a maximum load power of 400 mW. This sets an upper limit to the value of $|G|$.
- How to choose C_{OUT} ? At the lowest frequency of interest, we want the magnitude of the C_{OUT} impedance to be “small”. Let’s define “small” as less than $R_{LOAD}/10$. Choose C_{OUT} . Show all work!

3) Design a non-inverting voltage amplifier to drive a DC motor. The design requirements are the following:

- The DC motor is rated at 6V with a stall current of 1.8 A. **Design for a max load current = 0.9A.**
- The input signal is a DC voltage between -0.5V and +0.5V.

The design constraints are the following:

- Q1 must be a MPSA29 or TIP110 Darlington transistor (see Fig. 3).
 - NOTE: The pnp versions are the MPSA63 and TIP115.
- V_{CC} must be 4.5, 6, 9, or 12V.

- The op amp is the LF356.
- All resistors are standard 5% tolerance.

- Compute the max load voltage and current.
- Perform a “quick” analysis to find the minimum V_{CC} **and then choose a V_{CC}** (this may need to be changed later). NOTE: For a Darlington, “quick” parameters are $V_{BE} = 1.4V$, $\beta = 2500$, and $V_{CE(sat)} = 0.7V$.
- Choose Q1 and Q2. Show all work! Hint #1: Assume “quick” analysis parameters when computing power dissipation in Q1! Hint #2: As always, you can ignore R2 current since it is usually much smaller than the load current. Hint #3: The 2N4401 should work. If you need a heat sink, then you MUST compute the necessary θ_{SA} .

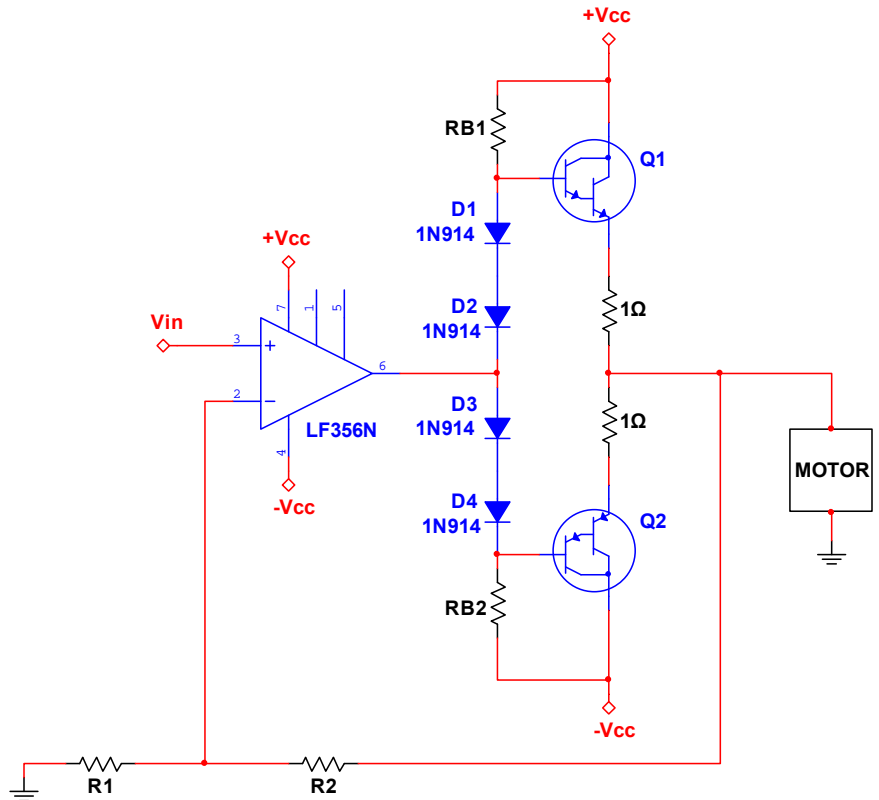


Fig. 3: Non-inverting amplifier with Darlington Class AB output stage.

- Choose RB1 and RB2. Pick standard 5% values. Hint: Around 1 kohm.
- Show that the op amp can provide the required output voltage and current. **If it does not, then you must increase V_{CC} to a higher value and repeat part (c) and (d).**
- Choose R1 and R2. Remember that $G = 1 + (R2/R1)$ for a non-inverting amplifier. Your final gain should produce a maximum output voltage that is within +/- 5% of 6V.

C. Real op amp effects

- The advantage of a non-inverting amplifier is the huge input impedance (well over 10 Mohm!). However, one still has to be careful about voltage errors!
 - Suppose $V_{SENSOR} = 0$. Given the LF356 (not the LF356B) op amp’s worst-case values for $I_{in(bias)}$, $I_{in(os)}$, and $V_{in(os)}$, compute the output voltage offset due to each parameter.
 - Is the main source of error due to input bias current, input offset current, or input offset voltage?
 - What is the worst-case output voltage offset?

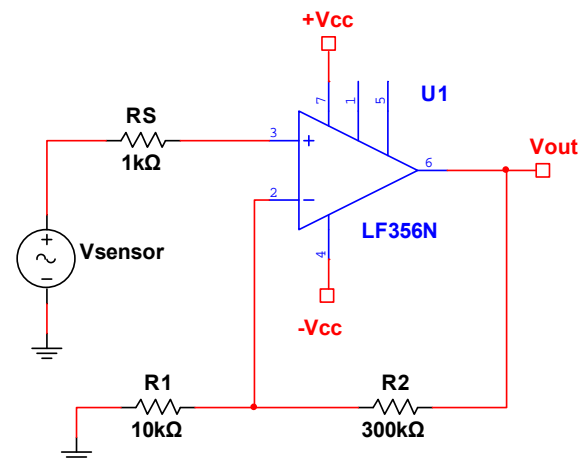


Fig. 4: Worst-case output voltage is the sum of the magnitudes of all three output errors!

- 5) The large input impedance of emitter followers make them useful as voltage buffers. However, they do have some drawbacks for small-signal DC applications ...
- Consider the emitter follower in Fig. 5a. Suppose V_{IN} is a triangle waveform from 0 to 1V. Assume $V_{BE} = 0.7V$ for the npn transistor. Sketch both V_{IN} and V_{LOAD} – you should find they are quite different from each other! ☹
 - A much better circuit is shown in Fig. 5b. Use the Golden Rules to derive an expression for V_{OUT} in terms of V_{SENSOR} .
 - What is the purpose of R? Choose the appropriate 5% resistor value for R.
 - Assuming the 741C op amp (worst-case parameters) and your choice of resistor R from part (c), compute the worst-case output error of the voltage buffer.

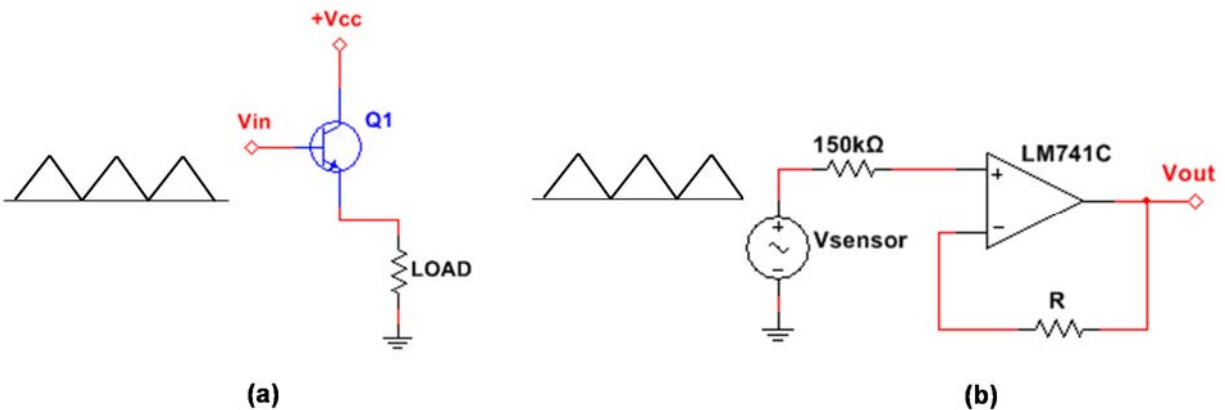


Fig. 5: (a) Emitter follower (b) Op amp follower using an LM741C.

- 6) Design a DC inverting amplifier with an input impedance of at least $R_{IN} = 10 \text{ kohm}$ and a gain of at least $G = -50$ (e.g. $G = -51$ is OK but $G = -49$ is not). Use an LF411 op amp (typical parameters). Also use standard 5% resistors.
- Determine R1 and R2.
 - Suppose V_{IN} comes from a sensor with an output impedance of 1 kohm. Compute the appropriate value for R3.
 - What is the expected bandwidth from this amplifier?

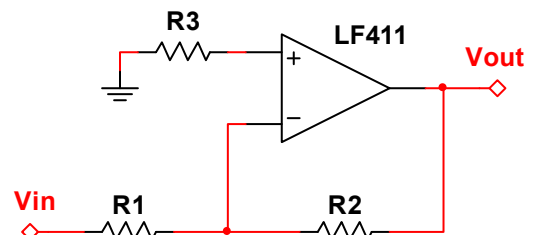


Fig. 6: DC inverting amplifier using an LF411.

D. Rise Time vs. Bandwidth

- 7) The output frequency response of most op amps can be described with a first-order low-pass filter. Consider a simple RC circuit. Suppose the input V_{IN} is a step function of amplitude V_O . The output voltage V_{OUT} does not change instantaneously! Instead, the output is given by $V_{OUT}(t) = V_O(1 - e^{-t/RC})$. The rise time can be defined as $T_R = T_{90} - T_{10}$, which is the time difference between V_{OUT} reaching $0.1V_O$ and $0.9V_O$.
- Solve the above equation to determine T_{10} , which is when $V_{OUT} = 0.1V_O$.
 - Solve the above equation to determine T_{90} , which is when $V_{OUT} = 0.9V_O$.
 - Show that $T_R = T_{90} - T_{10} = \ln(9) \cdot RC = 2.2RC$.

d) Using $f_c = 1/(2\pi RC)$, show that $T_R = 0.35/f_c$. NOTE: f_c is the -3dB bandwidth of the low-pass filter.

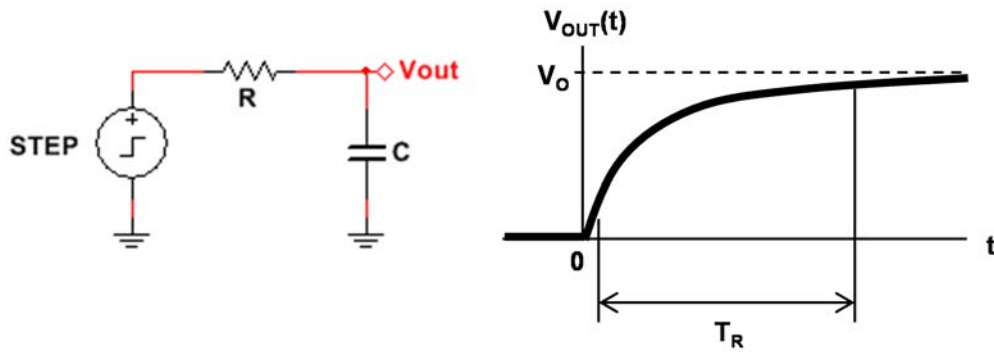


Fig. 7: Voltage waveform for a capacitor charged by a step voltage.

8) Consider an LM741 non-inverting amplifier with a gain $G = +26$ dB. The input V_{IN} is a 20 mV_{PP} square wave at 20 kHz. Ideally, the op amp output V_{OUT} is a perfect square wave. In reality, V_{OUT} takes a certain amount of time to swing up and down. See the course website for the LM741 data sheet.

- Compute the small-signal bandwidth and associated rise time T_R .
- Based on the LM741 slew-rate, compute the slew-rate limited rise time T_{SR} .
- Is your amplifier limited by small-signal bandwidth or slew rate?
- Sketch the amplifier output for 100 μ s. Label important features such as rise and fall times!

Note: If the amplifier is bandwidth limited, the V_{OUT} edges have “exponential decay”. If the amplifier is slew-rate limited, the V_{OUT} edges have a linear ramp shape.

9) Consider an LF411 inverting amplifier with a gain $|G| = +30$ dB. The input V_{IN} is a 200 mV_{PP} sine wave at 300 kHz. See the course website for the LF411 data sheet.

- Compute the large-signal bandwidth.
- Compute the small-signal bandwidth.
- Is the amplifier limited by slew-rate or small-signal bandwidth?