

# Lecture 9: MOSFET Switches

0. Review

1. MOSFET Intro

2. MOSFET Switch Analysis

3. MOSFET Switch Design

• PreLab 4 due Thu

• HW4 due Fri (Oct 25)

• Exam 1 re-do (counts as HW)  
due next Tue (Oct 29)

• Lab 3 report due Nov 4 (Mon)

Textbook Reading: 12-4 Enhancement Mode MOSFET

5 Ohmic region

8 Power FETs

9 High-side MOSFET load switches

# 0. Review

## Step 1

Know your load: current, voltage, etc

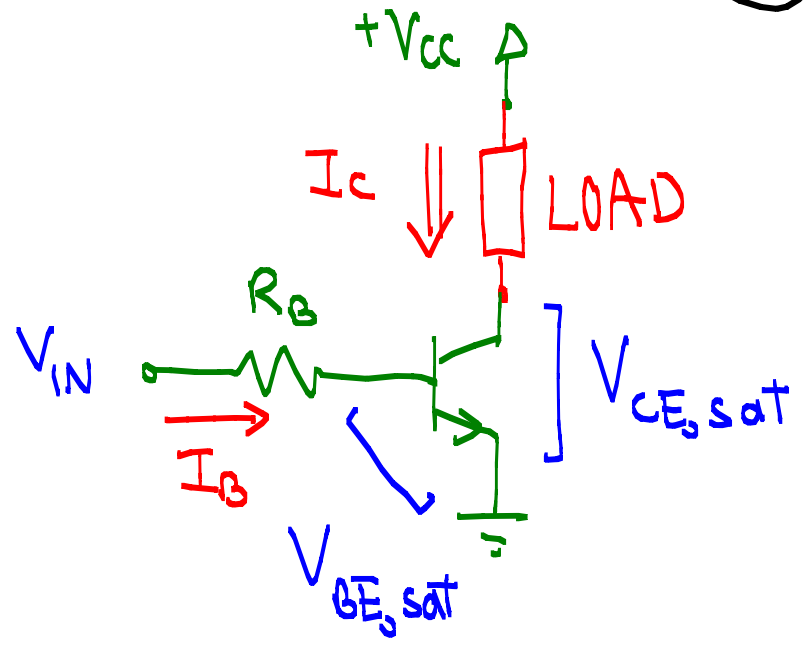
## Step 2

Wisely choose the transistor

↳ check  $\max I_c$ ,  $\max V_{CE}$ ,  $T_J$

## Step 3

Properly saturate the transistor

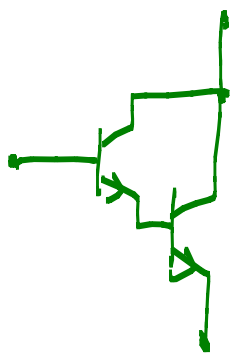


(A)  $V_{CE} = V_{CE,sat}$

(B)  $I_B \approx \frac{I_C}{10}$   
Single BJT



or  $I_B \approx \frac{I_C}{250}$   
Darlington



# 1. MOSFET Intro

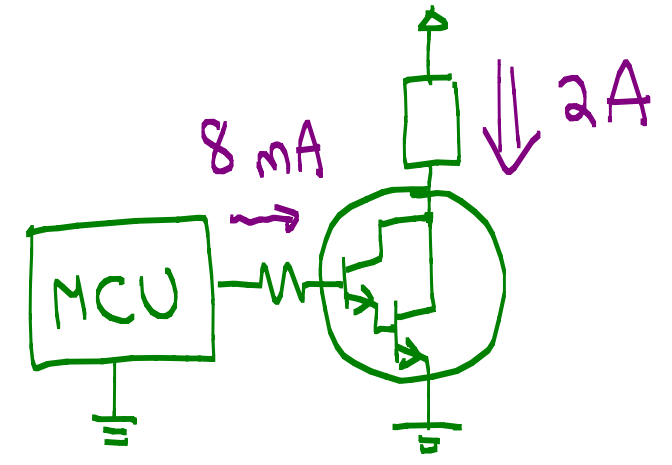
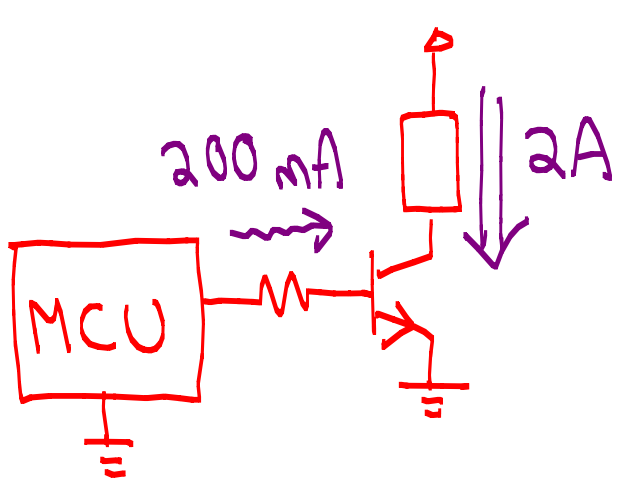
• BJT switches are very useful, but some issues to consider:

## ① Base Current

When  $I_c$  is large ( $> 1A$ )

$$\Rightarrow I_b \sim \frac{1}{10} I_c > 100mA$$

Arduino will burn out! ☹️

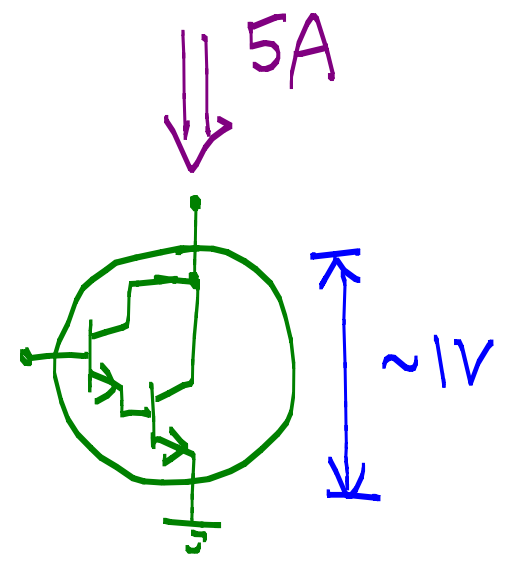


★ Darlington is good choice for  $I_c \sim$  several amps

## ② Power Dissipation

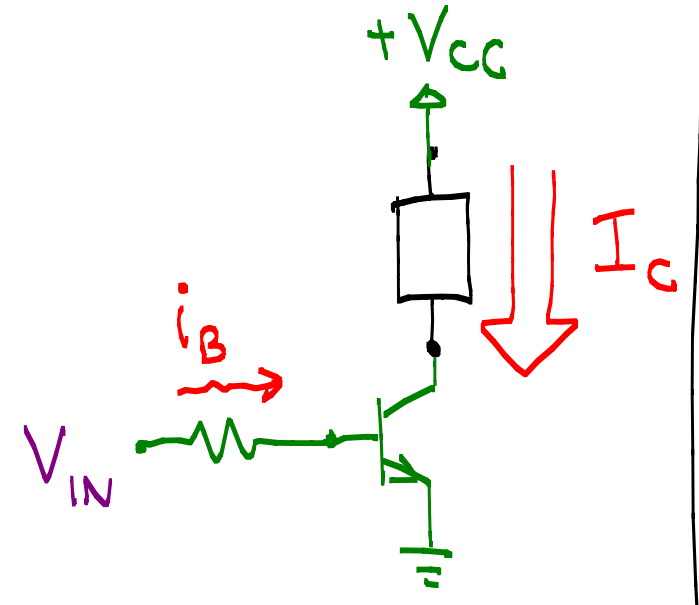
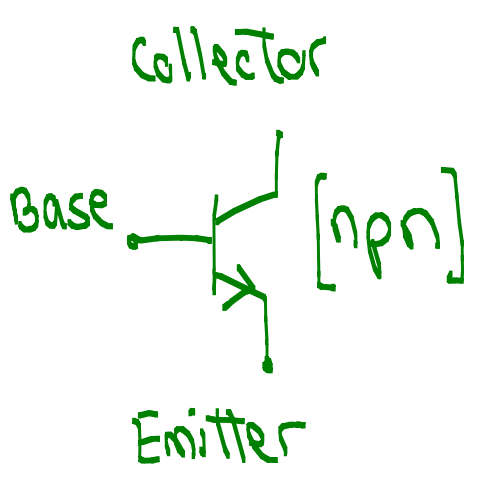
$$P = I_b V_{BE} + I_c V_{CE}$$

Can be  $\sim 1V$



$P \sim 5W$   
BJT gets HOT!

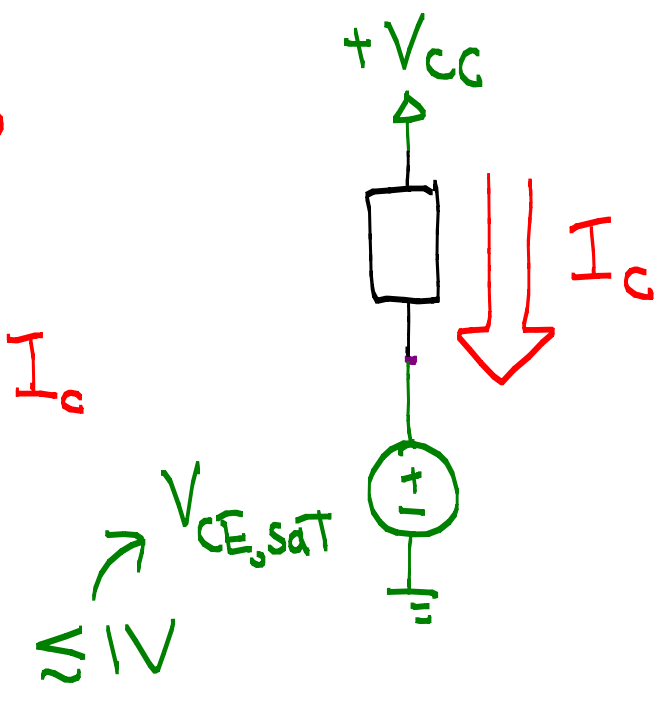
# BJT: Bipolar Junction Transistor



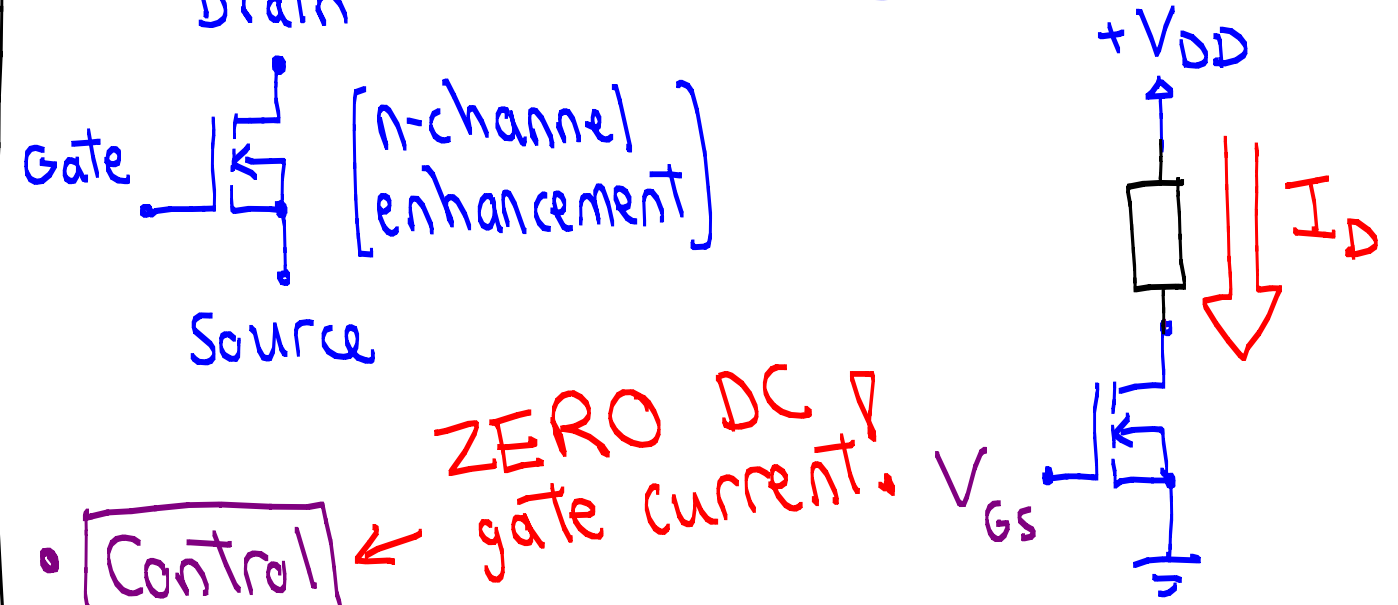
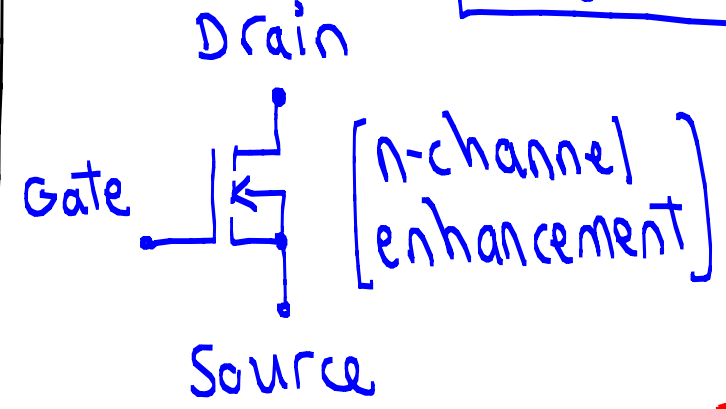
- Control  
Base current  $i_B$

- Load  
Collector current  $I_C$

- Mode  
Saturation



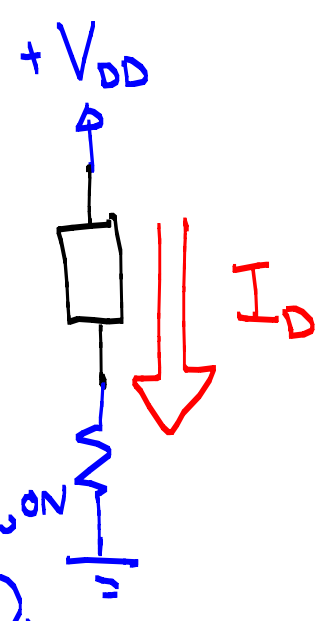
# MOSFET: Metal Oxide Semiconductor Field Effect Transistor



- Control  
ZERO DC gate current!  
Gate Source voltage  $V_{GS}$

- Load  
Drain current  $I_D$

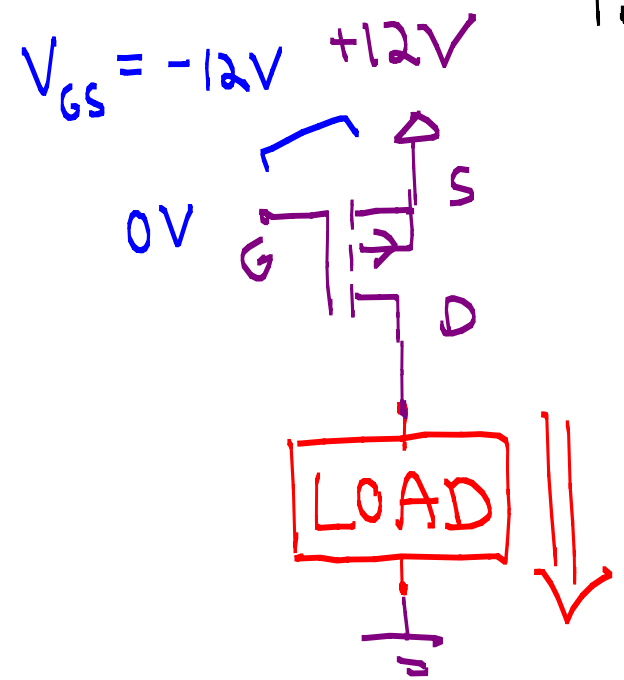
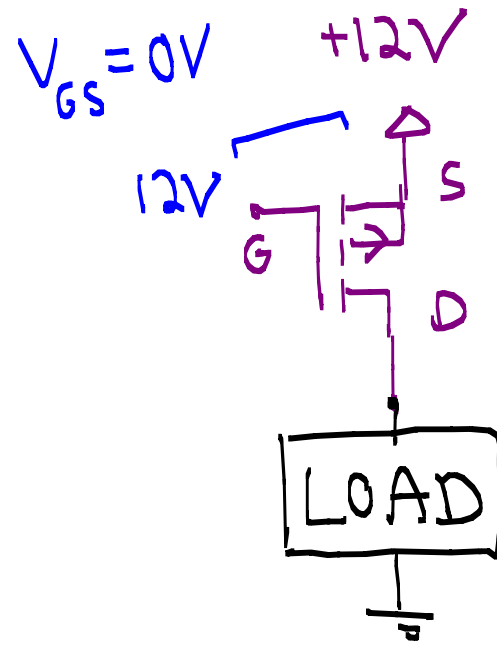
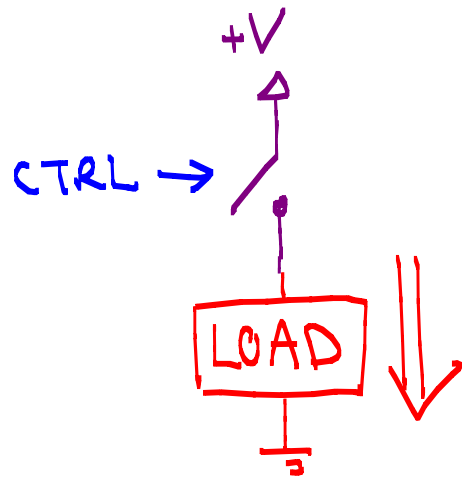
- Mode  
Ohmic (linear) region  $\approx R_{DS,ON} \approx \text{few } \Omega$



# Low-side vs. High-side Switch

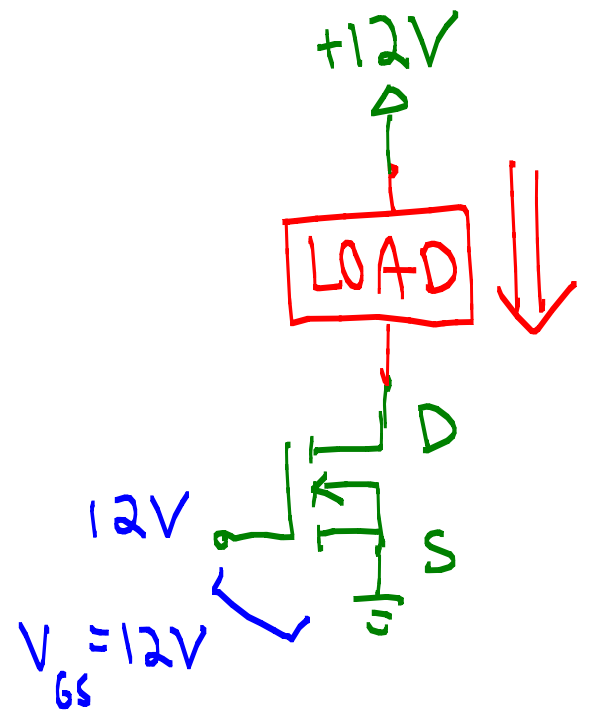
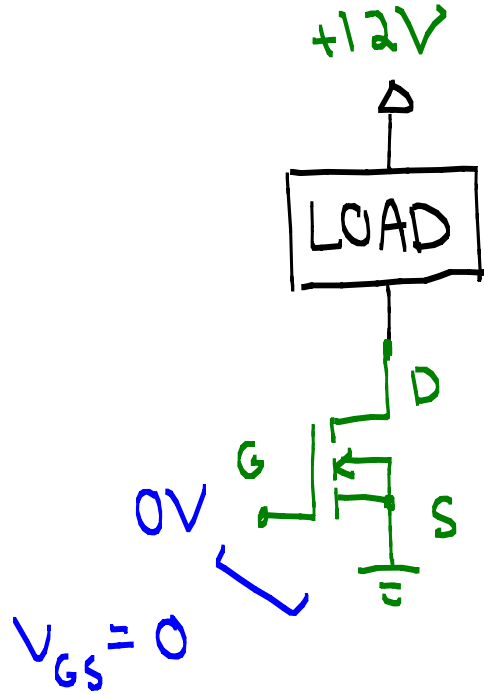
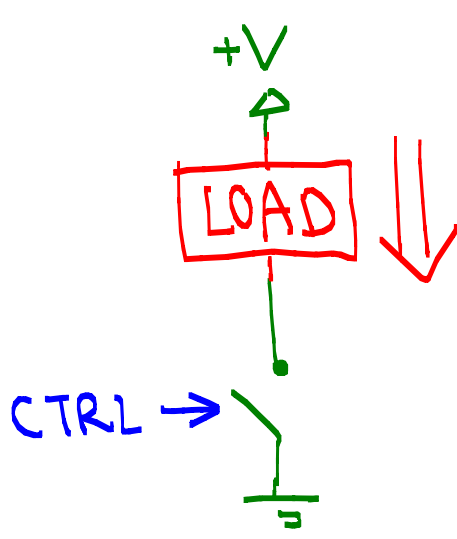
## High-side (p-ch)

ON when  $V_{GS}$  is negative



## Low-side (n-ch)

ON when  $V_{GS}$  is positive



• MOSFET Properties : 2 major ones

①  $V_{GS}$  : Gate-source voltage

★ Threshold :  $V_{GS} \gg V_{GS,TH}$  (ON)

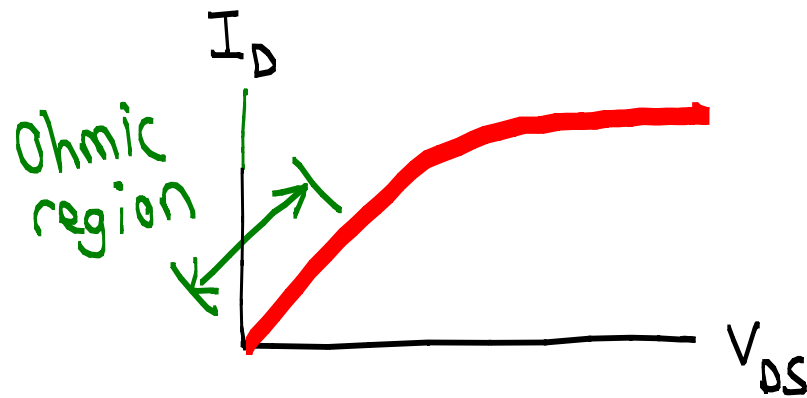
$V_{GS} \approx V_{GS,TH}$  (Barely on)

$V_{GS} < V_{GS,TH}$  (OFF)

②  $R_{DS,ON}$  : Drain-source on-resistance

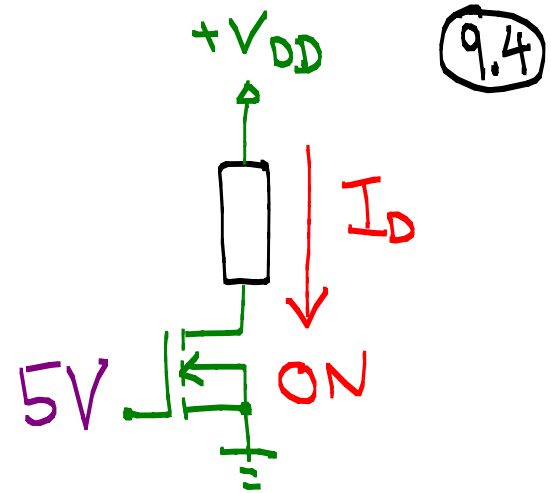
→ Requires operation in ohmic region

( $I_D$  cannot be too large!)



Small signal MOSFET

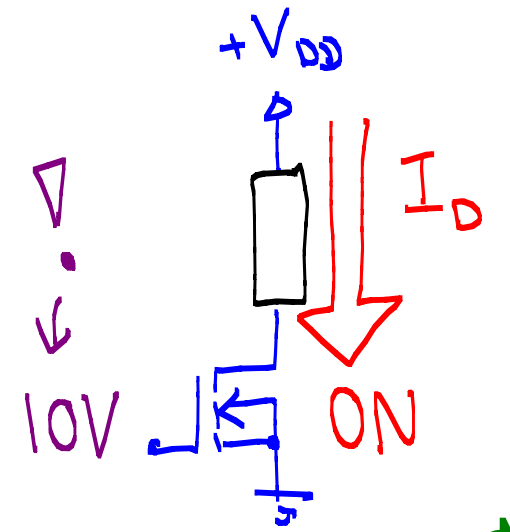
e.g. 2N7000  
 $V_{GS,TH} \sim 2V$



9.4

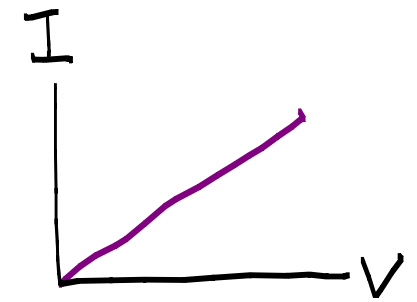
Power MOSFET

e.g. IRF510  
 $V_{GS,TH} \sim 5V$



Resistor

$I = \frac{1}{R} V$



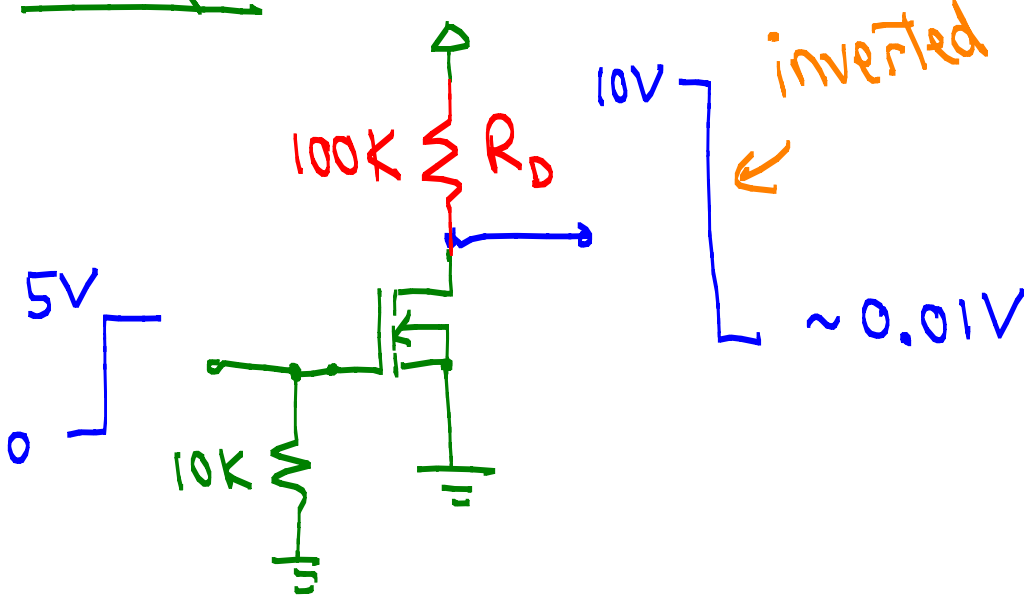
Q: How to convert 0-5V logic to higher voltage (e.g. 10V)?

A: Make a logic level shifter using...

$$V_{GS} = \begin{cases} 0 & \text{(OFF)} \\ -10V & \text{(ON)} \end{cases} \quad 9.5$$

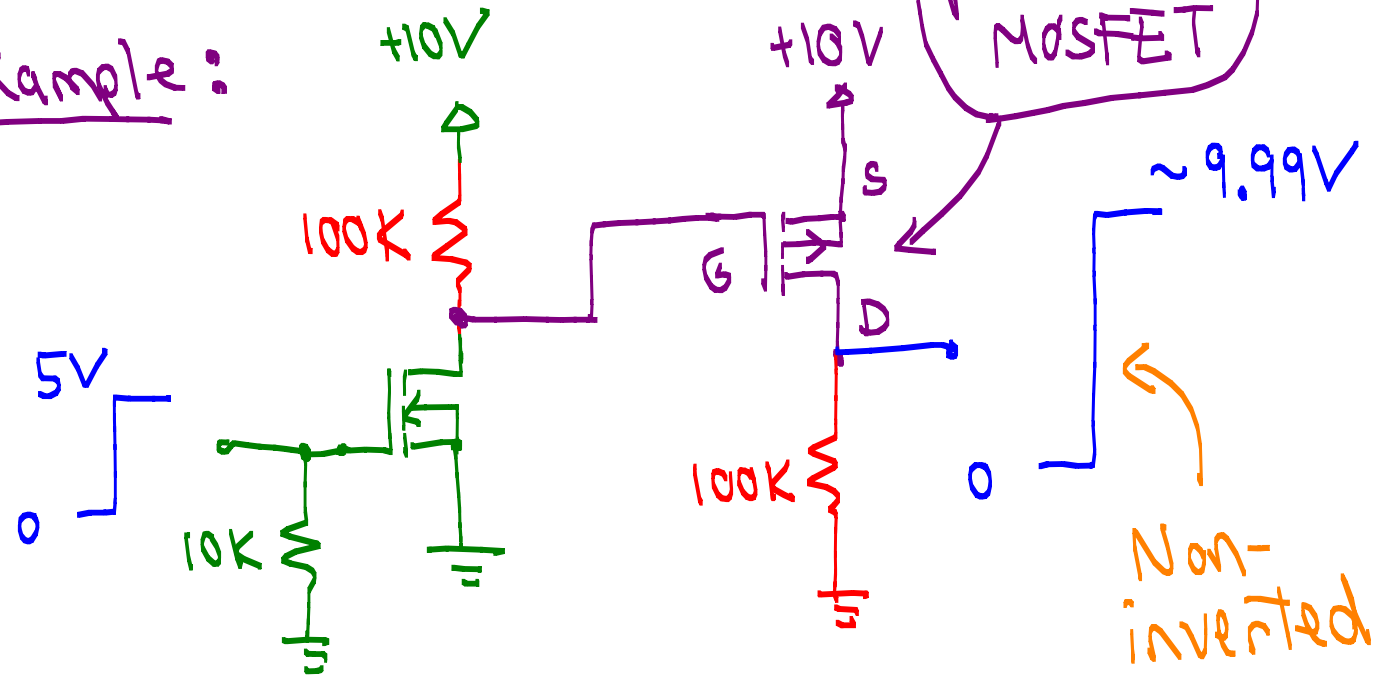
**One MOSFET**

Example: +10V



**Two MOSFETS**

Example:

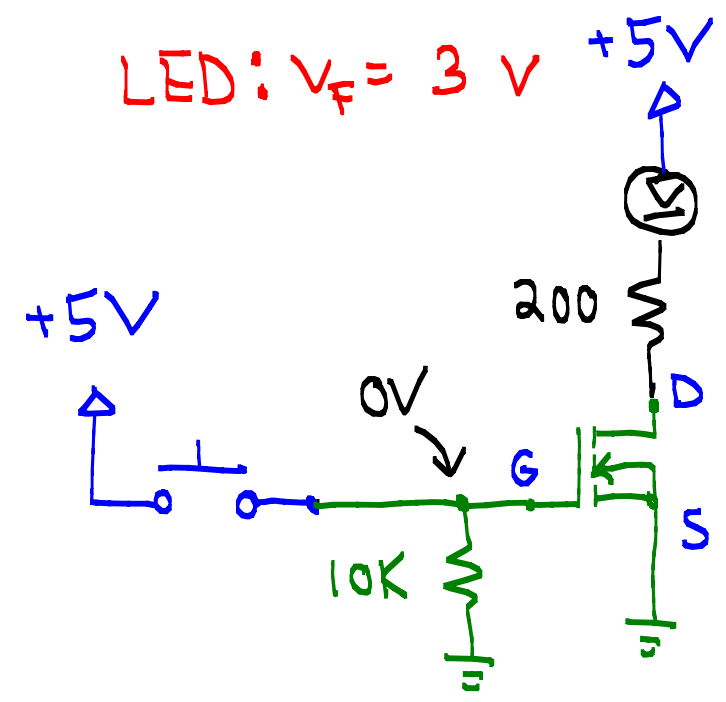


$R_D$ value:	100K	10K	1K
Power dissipation:	Low	Med	High
Speed:	SLOW (~100µs)	MED (~10µs)	FAST (~1µs)

# 2. MOSFET Switch Analysis ECE248 style

## • Example: LED Driver

MOSFET Properties:  $V_{GS,TH} = 2.4V$ ,  $R_{DS,ON} = 3\Omega$   $\left\{ \begin{array}{l} V_{GS} = 5V \\ I_{D,ON} = 250mA \end{array} \right.$

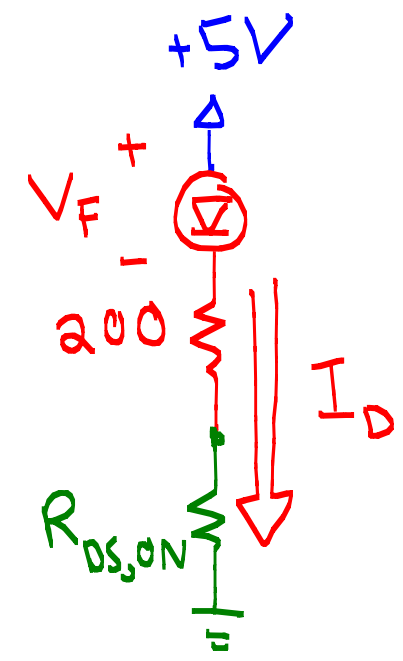
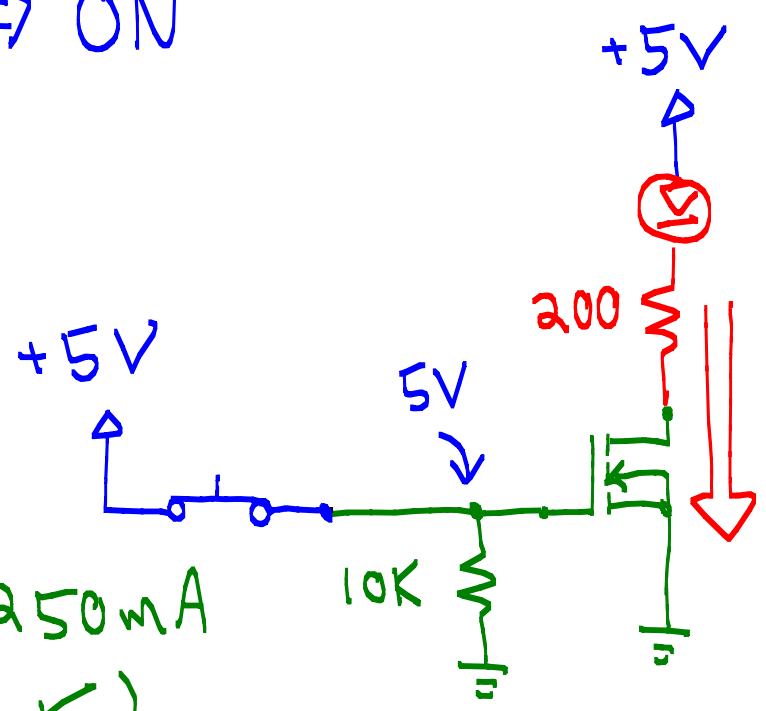


• Open push button:  $V_{GS} = 0V < 2.4V \Rightarrow OFF$

• Closed push button:  $V_{GS} = 5V > 2.4V \Rightarrow ON$

KVL:  $5 - \boxed{V_F} - I_D \cdot 200 - I_D \cdot \boxed{R_{DS,ON}} = 0$

$\Rightarrow I_D = \frac{5 - 3V}{200 + 3\Omega} = .0099A = 9.9mA < 250mA$   
(ohmic ✓)



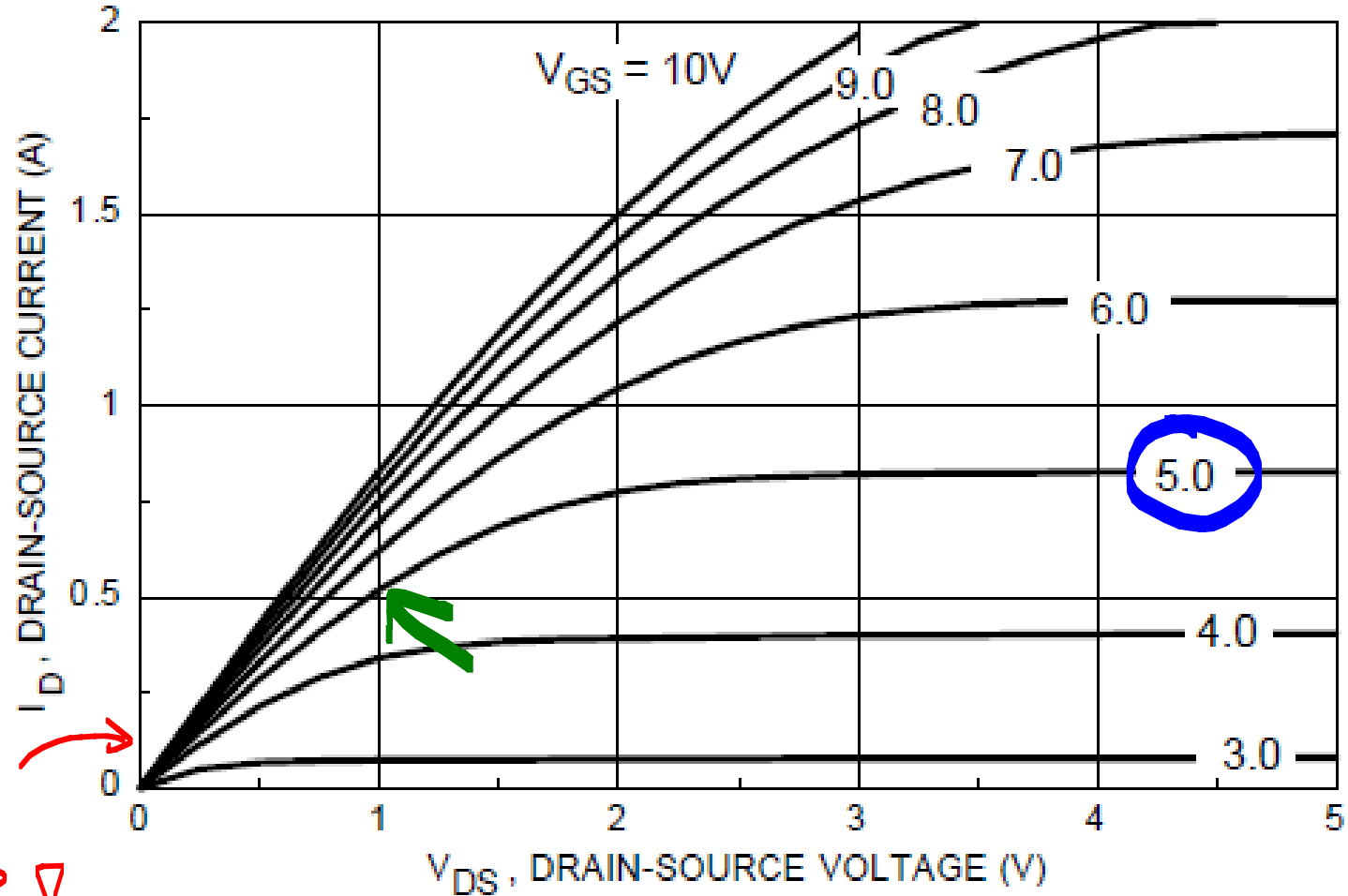
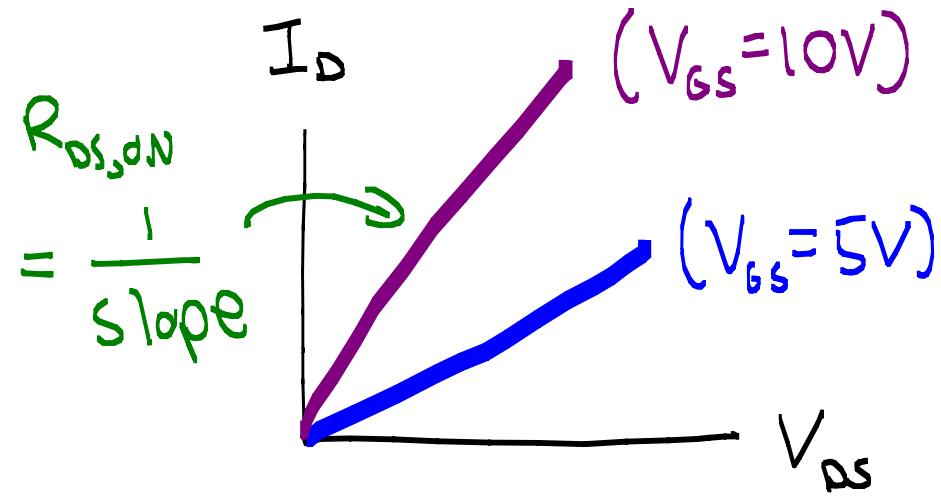


**ECE 363 style analysis**

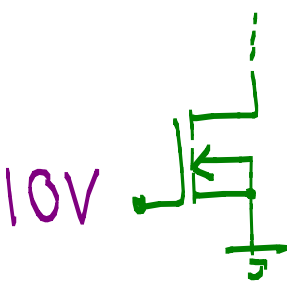
MOSFET data sheet has a plot like this:

9.7

$R_{DS,ON}$  depends on  $V_{GS}$ !



I-V curve for  $V_{GS} = 5V$



$0.010A$  is down here!

(ohmic region ✓)

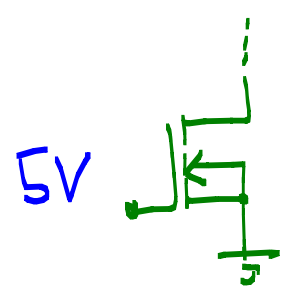


Figure 1. On-Region Characteristics

$$R_{DS,ON} = \frac{1}{\text{slope}} \approx \frac{1}{.5A/1V} = 2\Omega$$

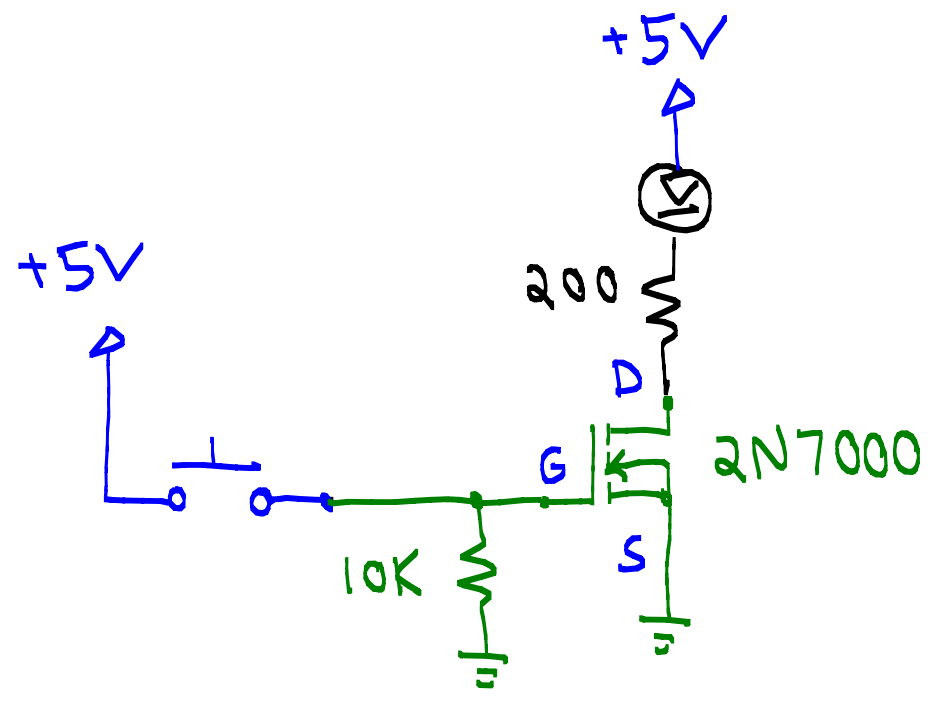
• From data sheet:

$V_{GS,TH} = 2.1V$ ,  $R_{DS,ON} = 2 \Omega$

10mA is in ohmic region ✓

• Push button open:

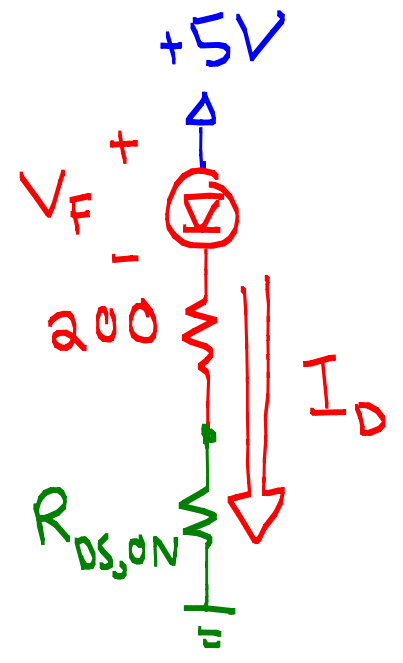
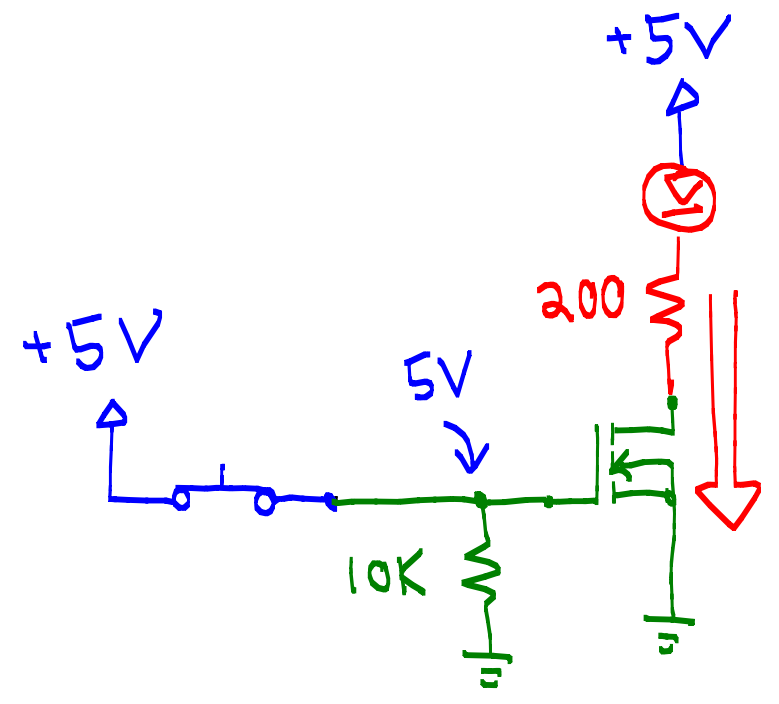
$V_{GS} = 0V < 2.1V$  OFF



• Push button closed:

$5 - V_F - I_D \times 200 - I_D \times 2 = 0$

$I_D = \frac{5 - 3V}{200 + 2} = 0.0099 A = 9.9 mA$



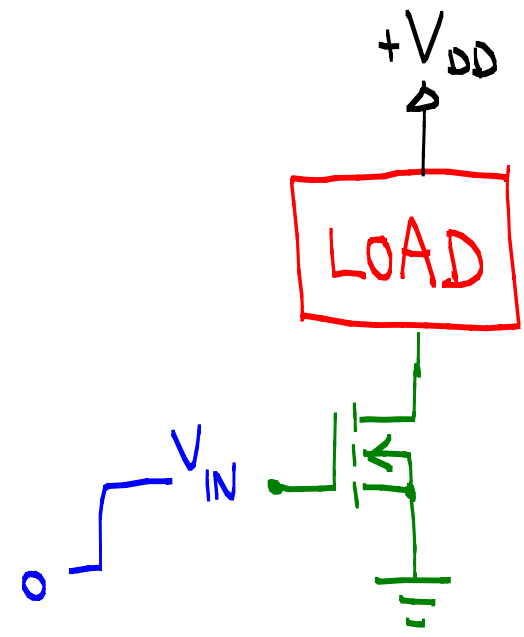
### 3. MOSFET switch design

**STEP 1** Know your load  $\rightarrow$  Voltage  
 $\rightarrow$  Current

**STEP 2** Wisely choose the MOSFET

- ① Max  $I_D$ , max  $V_{DS}$ , max  $V_{GS}$
- ②  $V_{GS}$  and  $R_{DS(on)}$  are OK
- ③ Max  $T_J$  is OK

**STEP 3** When MOSFET is on, load is properly working

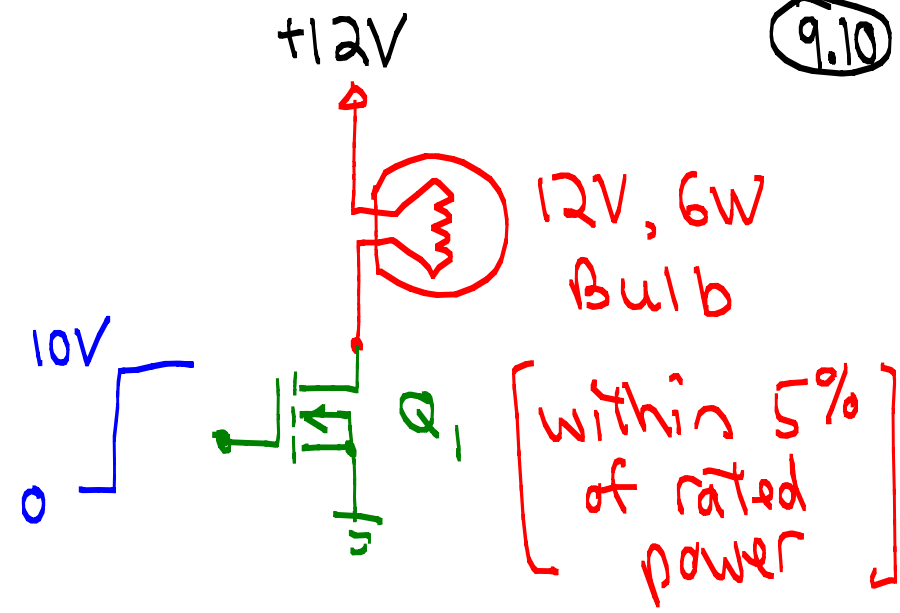


Design example using typical properties:

STEP 1 Load properties

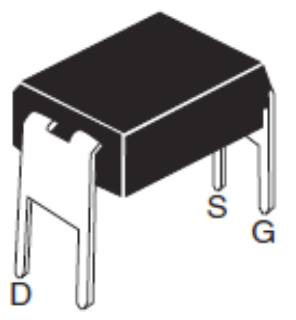
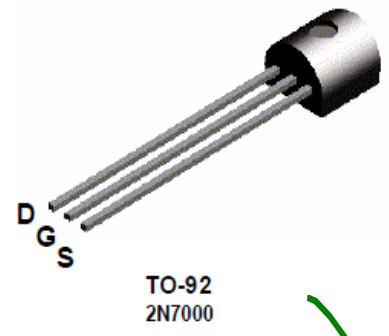
I = 6W / 12V = 0.5A \*2 -> 1A rating

R = (12V)^2 / 6W = 24 Ohm



STEP 2 Choose MOSFETs

Q1:



	Max I <sub>D</sub>	V <sub>GS</sub>	V <sub>DS</sub>	Rated P (no Hs) (w/Hs)
2N7000	200mA	±20V	60V	0.4W
IRFD120	1.3A	±20V	100V	1.3W

• Threshold  $V_{GS}$

9.11

SPECIFICATIONS ( $T_J = 25\text{ }^\circ\text{C}$ , unless otherwise noted)						
PARAMETER	SYMBOL	TEST CONDITIONS	MIN.	TYP.	MAX.	UNIT
Static						
Drain-Source Breakdown Voltage	$V_{DS}$	$V_{GS} = 0\text{ V}, I_D = 250\text{ }\mu\text{A}$	100	-	-	V
$V_{DS}$ Temperature Coefficient	$\Delta V_{DS}/T_J$	Reference to $25\text{ }^\circ\text{C}, I_D = 1\text{ mA}$	-	0.13	-	V/ $^\circ\text{C}$
Gate-Source Threshold Voltage	$V_{GS(th)}$	$V_{DS} = V_{GS}, I_D = 250\text{ }\mu\text{A}$	2.0	-	4.0	V
Gate-Source Leakage	$I_{GSS}$	$V_{GS} = \pm 20\text{ V}$	-	-	$\pm 100$	nA
Zero Gate Voltage Drain Current	$I_{DSS}$	$V_{DS} = 100\text{ V}, V_{GS} = 0\text{ V}$	-	-	25	$\mu\text{A}$
		$V_{DS} = 80\text{ V}, V_{GS} = 0\text{ V}, T_J = 150\text{ }^\circ\text{C}$	-	-	250	
Drain-Source On-State Resistance	$R_{DS(on)}$	$V_{GS} = 10\text{ V}$   $I_D = 0.78\text{ A}^b$	-	-	0.27	$\Omega$

Clearly,  $V_{GS} = 10\text{ V} \Rightarrow V_{GS,th}$  ✓

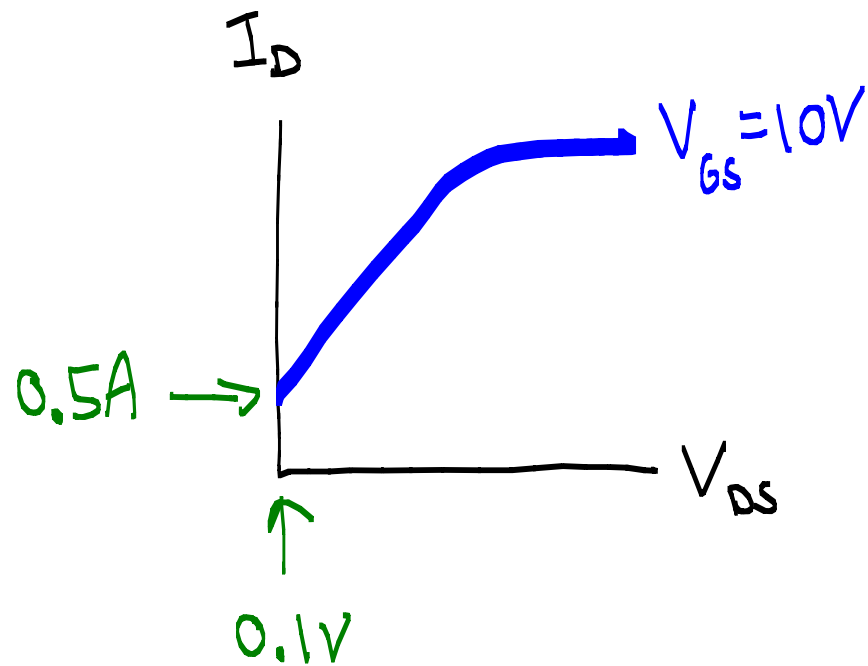
Typical  $R_{DS(on)}$ ?

Worst Case Values

Max  $V_{GS,th} = 4\text{ V}$

Max  $R_{DS(on)} = 0.27\text{ }\Omega$

Typical  $R_{DS(on)}$  @  $V_{GS} = 10V$ :



Typical  $R_{DS(on)} \approx \frac{0.1V}{0.5A} = \underline{\underline{0.2\Omega}}$

• Ohmic region?

Clearly in ohmic region



$I_D$ , Drain Current (Amps)

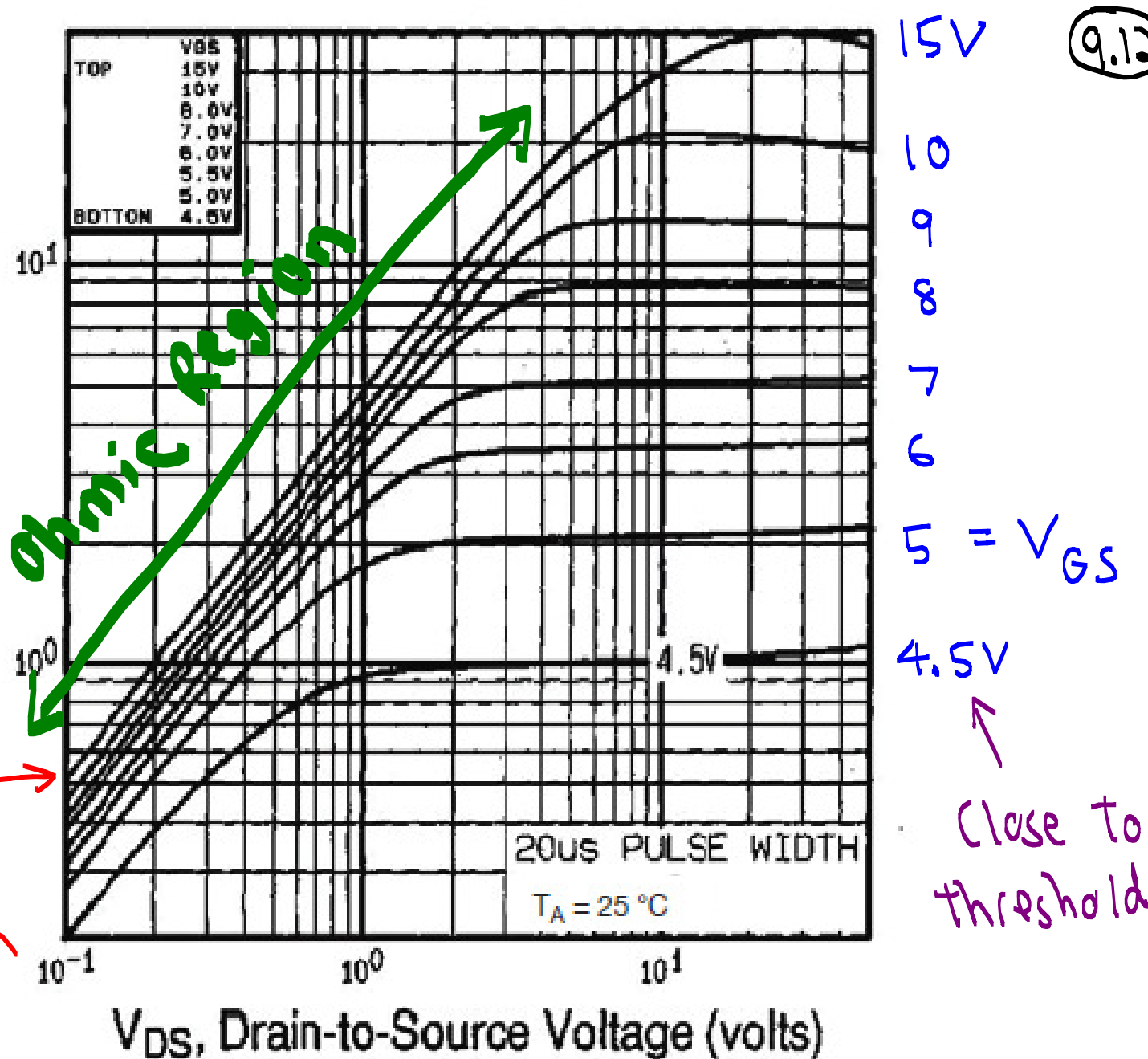


Fig. 1 - Typical Output Characteristics,  $T_A = 25^\circ C$

9.12

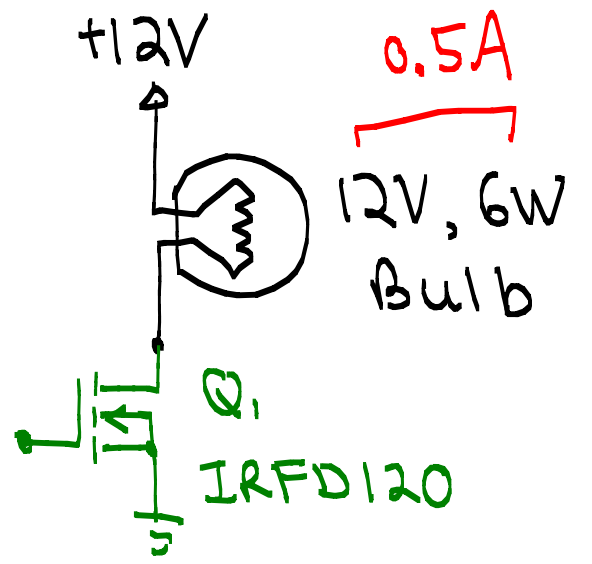
•  $V_{GS} = 10V \rightarrow Q_1$  is ON

$$I_D = \frac{12 - 0V}{24 + .2\Omega} = 0.496A$$

$$P = (.496A)^2 \cdot .2\Omega = \underline{.049W} \xrightarrow{\times 2} 0.1W$$

$$T_J = 25^\circ C + (.0492W) 120^\circ C/W = 31^\circ C < 85^\circ C$$

No heat sink needed.



**STEP 3** Confirm operation

Bulb current :  $I_D = \underline{.496A}$

Bulb power :  $P = (.496A)^2 (24\Omega) = \underline{5.9W}$  (< 2% of rated power) ✓

★ NOTE : MOSFETs can handle higher  $T_J$  than BJTs!

(175°C max)

(150°C max)