

1) (a) $V_- = V_+ = \underline{0}$

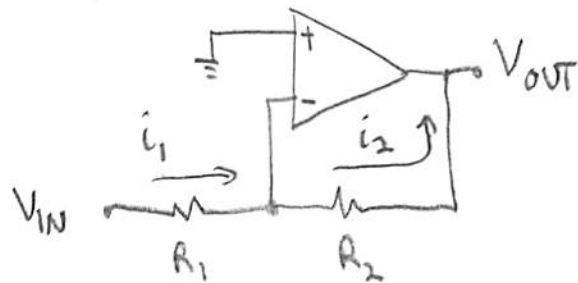
KCL at node V_- :

$$i_1 = i_2 + 0$$

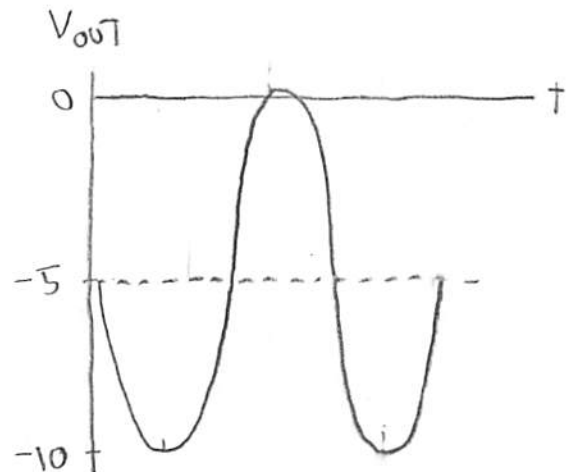
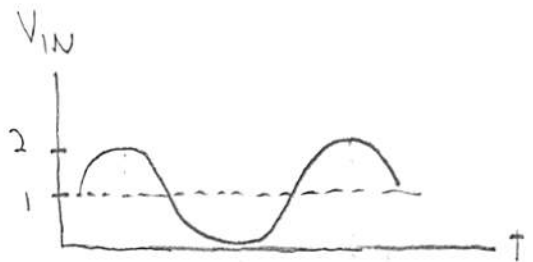
$$\frac{V_{IN} - 0}{R_1} = \frac{0 - V_{OUT}}{R_2} \Rightarrow \frac{V_{IN}}{R_1} = -\frac{V_{OUT}}{R_2}$$

+6

$$\frac{V_{OUT}}{V_{IN}} = -\frac{R_2}{R_1}$$



(b) $\frac{V_{OUT}}{V_{IN}} = -\frac{75K}{15K} = -5$
↑ invert!



+6

2) a) (+6)

$$V_- = V_+ = V_0$$

KCL at node V_- :

$$i_1 = i_2 + 0$$

$$\frac{V_{IN} - V_-}{R_1} = \frac{V_- - V_{OUT}}{R_2} \Rightarrow \frac{V_{IN} - V_0}{R_1} = \frac{V_0 - V_{OUT}}{R_2}$$

$$\frac{R_2}{R_1} V_{IN} - \frac{R_2}{R_1} V_0 - V_0 = -V_{OUT}$$

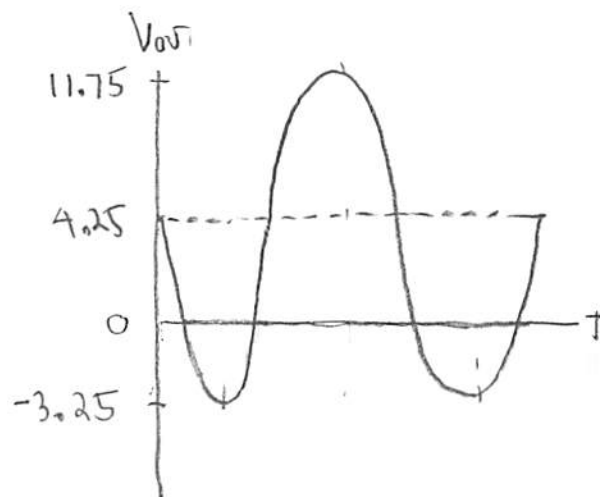
$$\Rightarrow V_{OUT} = \left(1 + \frac{R_2}{R_1}\right) V_0 - \frac{R_2}{R_1} V_{IN}$$

$$\textcircled{b} \quad V_{OUT} = \left(1 + \frac{75K}{10K}\right)(0.5V) - \frac{75K}{10K} V_{IN}$$

$$= \underbrace{4.25}_{\text{DC offset}} - \underbrace{7.5}_{\text{invert!}} V_{IN}$$

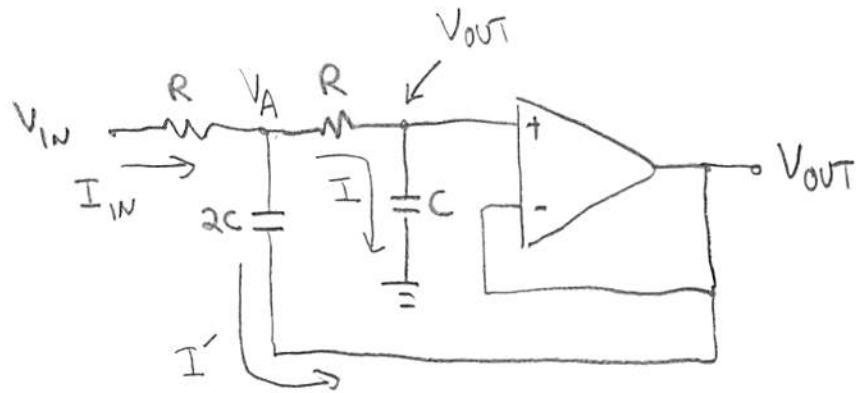


(+6)



3)

+12



(a) Rule 1: $V_+ = V_- = V_{OUT}$

$$I = \frac{V_A - V_{OUT}}{R} = \frac{V_{OUT}}{Z}, \quad Z = \frac{1}{j\omega C}$$

$$\Rightarrow V_A = \left(\frac{R}{Z} + 1\right) V_{OUT} \quad (1)$$

KCL at node A:

$$I_{IN} = I + I'$$

$$\frac{V_{IN} - V_A}{R} = \frac{V_{OUT}}{Z} + \frac{V_A - V_{OUT}}{\frac{1}{2}Z} \quad \frac{1}{j\omega 2C} = \frac{1}{2}Z$$

$$\begin{aligned} V_{IN} \frac{Z}{R} &= \frac{Z}{R} V_A + \cancel{V_{OUT}} + 2V_A - \cancel{2V_{OUT}} \\ &= \frac{Z}{R} \left(\frac{R}{Z} + 1\right) V_{OUT} + 2\left(\frac{R}{Z} + 1\right) V_{OUT} - V_{OUT} \\ &= \left(\cancel{1} + \frac{Z}{R} + 2\frac{R}{Z} + 2 - \cancel{1}\right) V_{OUT} \end{aligned}$$

$$\frac{V_{OUT}}{V_{IN}} = \frac{\frac{Z}{R}}{\frac{Z}{R} + 2 + 2\frac{R}{Z}} = \frac{1}{1 + 2\frac{R}{Z} + 2\frac{R^2}{Z^2}}$$

4

$$\text{let } Z = \frac{1}{j\omega C} \rightarrow \frac{1}{Z} = j\omega C, \quad \frac{1}{Z^2} = -\omega^2 C^2$$

$$\rightarrow \boxed{\frac{V_{OUT}}{V_{IN}} = \frac{1}{1 + 2j\omega RC - 2\omega^2 R^2 C^2}}$$

4)

(+12)

$$\frac{V_{OUT}}{V_{IN}} = \frac{1}{(1 - 2\omega^2 R^2 C^2) + j 2\omega RC}$$

$$\left| \frac{V_{OUT}}{V_{IN}} \right| = \frac{1}{\sqrt{(1 - 2\omega^2 R^2 C^2)^2 + (2\omega RC)^2}}$$

$$= \frac{1}{\sqrt{1 - 4\omega^2 R^2 C^2 + 4\omega^4 R^4 C^4 + 4\omega^2 R^2 C^2}}$$

$$= \frac{1}{\sqrt{1 + 4\omega^4 R^4 C^4}} = \frac{1}{\sqrt{1 + \underbrace{64 \pi^4 R^4 C^4}_{\frac{1}{f_c^4}} f^4}}$$

$\uparrow$
 $2\pi f$

$$\text{Let } f_c = \frac{1}{64^{1/4} \pi RC}$$

$$64^{1/4} = (8^2)^{1/4} = \sqrt{8} = 2\sqrt{2}$$

$$\rightarrow f_c = \frac{1}{2\sqrt{2} \pi RC}$$

$$\text{So, } \boxed{\left| \frac{V_{out}}{V_{in}} \right| = \frac{1}{\sqrt{1 + (f/f_c)^4}}} \leftarrow f_c = \frac{1}{2\sqrt{2} \pi RC}$$

$$5) \text{ When } f = f_c \rightarrow \left| \frac{V_{out}}{V_{in}} \right| = \frac{1}{\sqrt{1 + (1)^4}} = \frac{1}{\sqrt{2}}$$

+8

$$20 \log_{10} \frac{1}{\sqrt{2}} = \boxed{-3 \text{ dB}}$$

$$6) \quad 20 \log_{10} \left| \frac{V_{out}}{V_{in}} \right| = -20 \text{ dB}$$

+8

$$\left| \frac{V_{out}}{V_{in}} \right| = 10^{-20/20} = 0.1 = \frac{1}{\sqrt{1 + (f_{stop}/f_c)^4}}$$

$$0.1 = \frac{1}{1 + (f_{stop}/f_c)^4}$$

$$\frac{f_{stop}}{f_c} = (100 - 1)^{1/4}$$

$$f_{stop} = 99^{1/4} f_c = \boxed{3.15 f_c}$$

7) Instrumentation amplifier output is: $V_{out} = A_d \Delta V + A_{cm} V_{cm}$

$+12$ • $A_d = 25$
 $\Delta V = 50 \text{ mV} + (300 \mu\text{V R-wave}) \left\{ A_d \Delta V = 1.25 \text{ V} + (7.5 \text{ mV R-wave}) \right.$

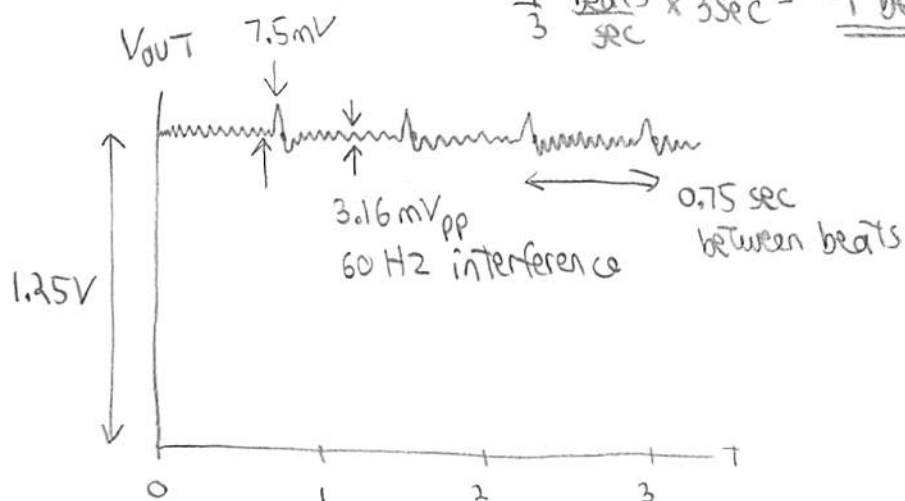
• $A_{cm} ?$ $\text{CMRR} = 20 \log_{10} \frac{A_d}{A_{cm}} \rightarrow \frac{A_d}{A_{cm}} = 10^{\text{CMRR}/20}$
 $A_{cm} = A_d 10^{-\text{CMRR}/20}$
 $= 25 \times 10^{-90/20} = \underline{\underline{7.9 \times 10^{-4}}}$

$V_{cm} = 2 \sin 2\pi f_0 t$
 $\uparrow 60 \text{ Hz} \Rightarrow A_{cm} V_{cm} = .00158 \sin 2\pi f_0 t$

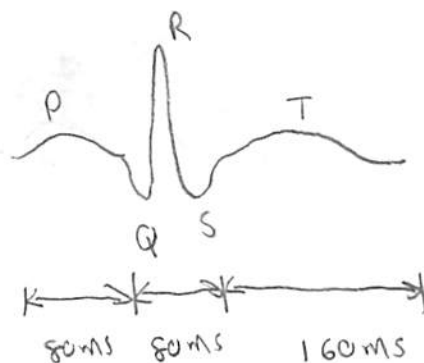
So, $V_{out} = 1.25 + (.0075 \text{ V R-wave}) + .00158 \sin 2\pi f_0 t$

80 beats per minute $\rightarrow \frac{80 \text{ beats}}{\text{min}} \times \frac{1 \text{ min}}{60 \text{ sec}} = \frac{4}{3} \frac{\text{beats}}{\text{sec}} \rightarrow 0.75 \text{ sec between beats}$

$\frac{4}{3} \frac{\text{beats}}{\text{sec}} \times 3 \text{ sec} = \underline{\underline{4 \text{ beats}}}$



8) PQRST waveform:



The bandwidth of a pulse is roughly given by:

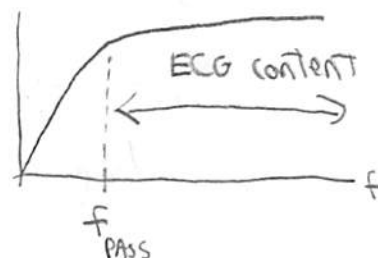
$$BW \sim \frac{1}{\text{duration}}$$

$$\text{P-wave: } BW \sim \frac{1}{.08s} = 12.5 \text{ Hz}$$

$$\text{QRS : } BW \sim \frac{1}{.08s} = 12.5 \text{ Hz}$$

$$\text{T-wave: } BW \sim \frac{1}{.16s} = 6.25 \text{ Hz}$$

we want $f_{\text{PASS}} < \text{smallest BW in PQRST waveform.}$
 $< 6.25 \text{ Hz}$

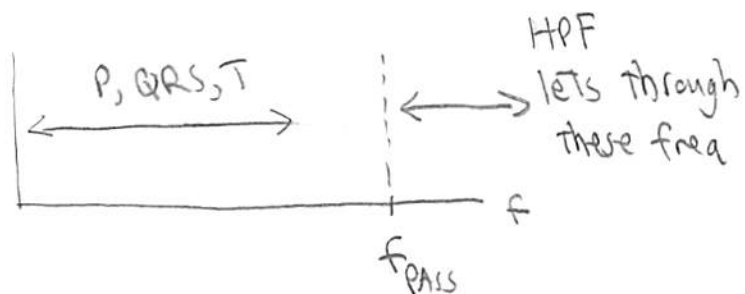


✱ $f_c = 1 \text{ Hz}$ is a good choice because $f_{\text{PASS}} = 2.07 \text{ Hz}$ is well below 6.25 Hz

• $f_c = 10 \text{ Hz}$ is a poor choice because $f_{\text{PASS}} = 20.7 \text{ Hz}$

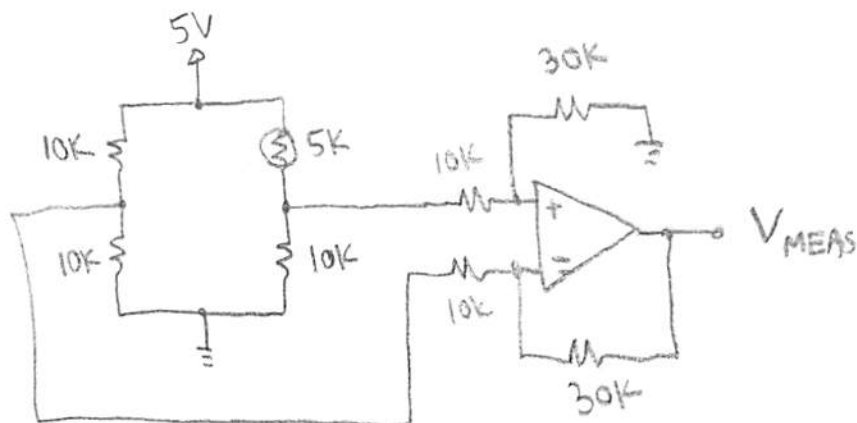
is above the bandwidth of P, QRS, and T portions!

⇓
ECG waveform is significantly affected by HPF.

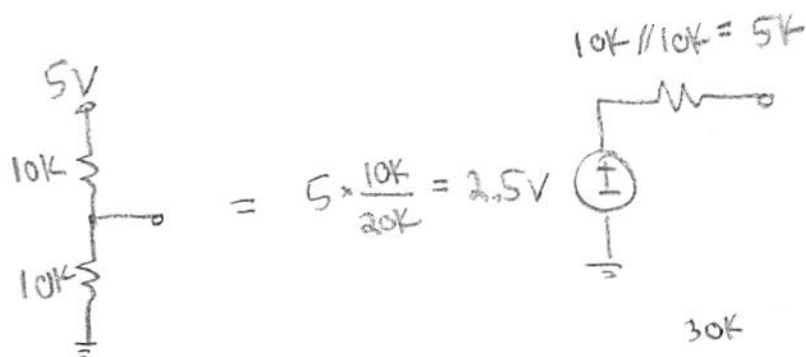
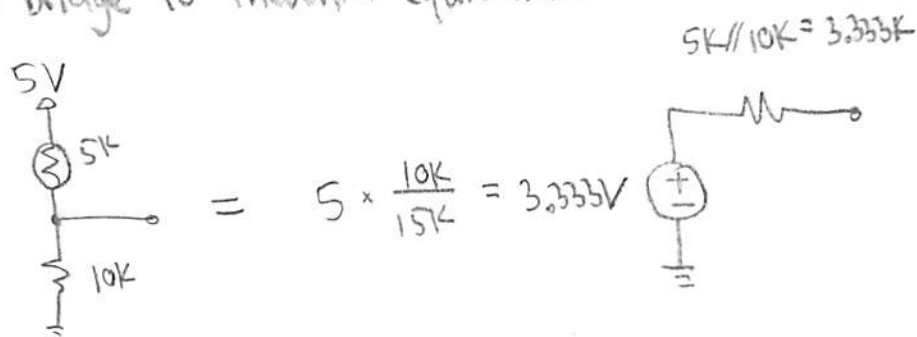


9)

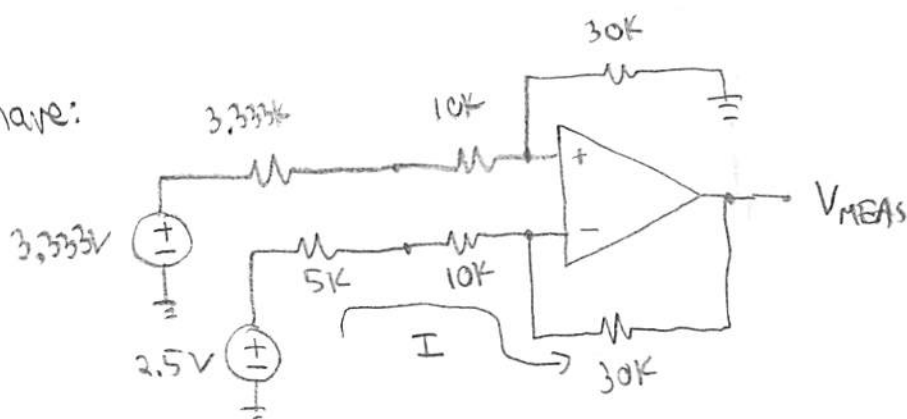
+12



Convert bridge to Thevenin equivalent:



We now have:



$$V_+ = (3.333V) \frac{30k}{3.333k + 10k + 30k} = \underline{\underline{2.31V}} = V_-$$

$$I = \frac{2.5V - 2.31V}{5k + 10k} = \underline{\underline{0.0267mA}}$$

9

$$\text{So, } V_{\text{MEAS}} = V_- - I \times 30\text{K} = 2.31\text{V} - (.01267\text{mA})(30\text{K}) = \boxed{1.93\text{V}}$$

An instrumentation amplifier with $A_d = 3$ would produce:

$$V_{\text{MEAS}} = 3 \times (3.333\text{V} - 2.5\text{V}) = \underline{\underline{2.5\text{V}}}$$

$$\text{Error} = \frac{1.93 - 2.5}{2.5} = -0.228 = \boxed{-22.8\%}$$