

Lecture 7: Instrumentation Amplifier

(Quiz)

0. Review

1. Inst Amp Basics

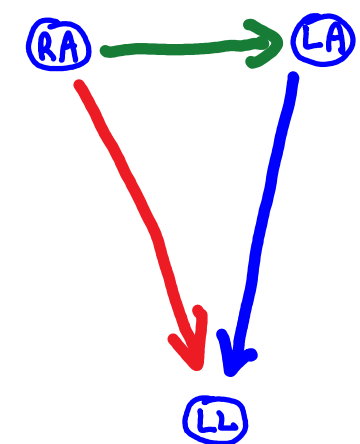
2. Common Mode Rejection Ratio
(CMRR)

- PreLab 3 due at lab session
- Thu (Jan 30): HW3
- Fri (Jan 31): Lab 2 report
- Exam #1 (Feb 6)!
 - HW 1, 2, 3 material
 - Lectures 1-8
 - Course website will have sample exam + solutions

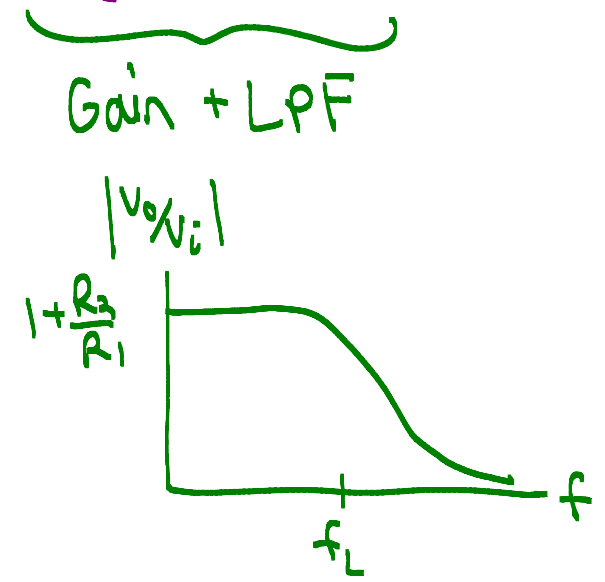
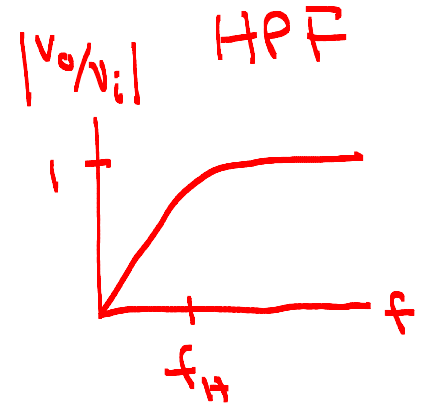
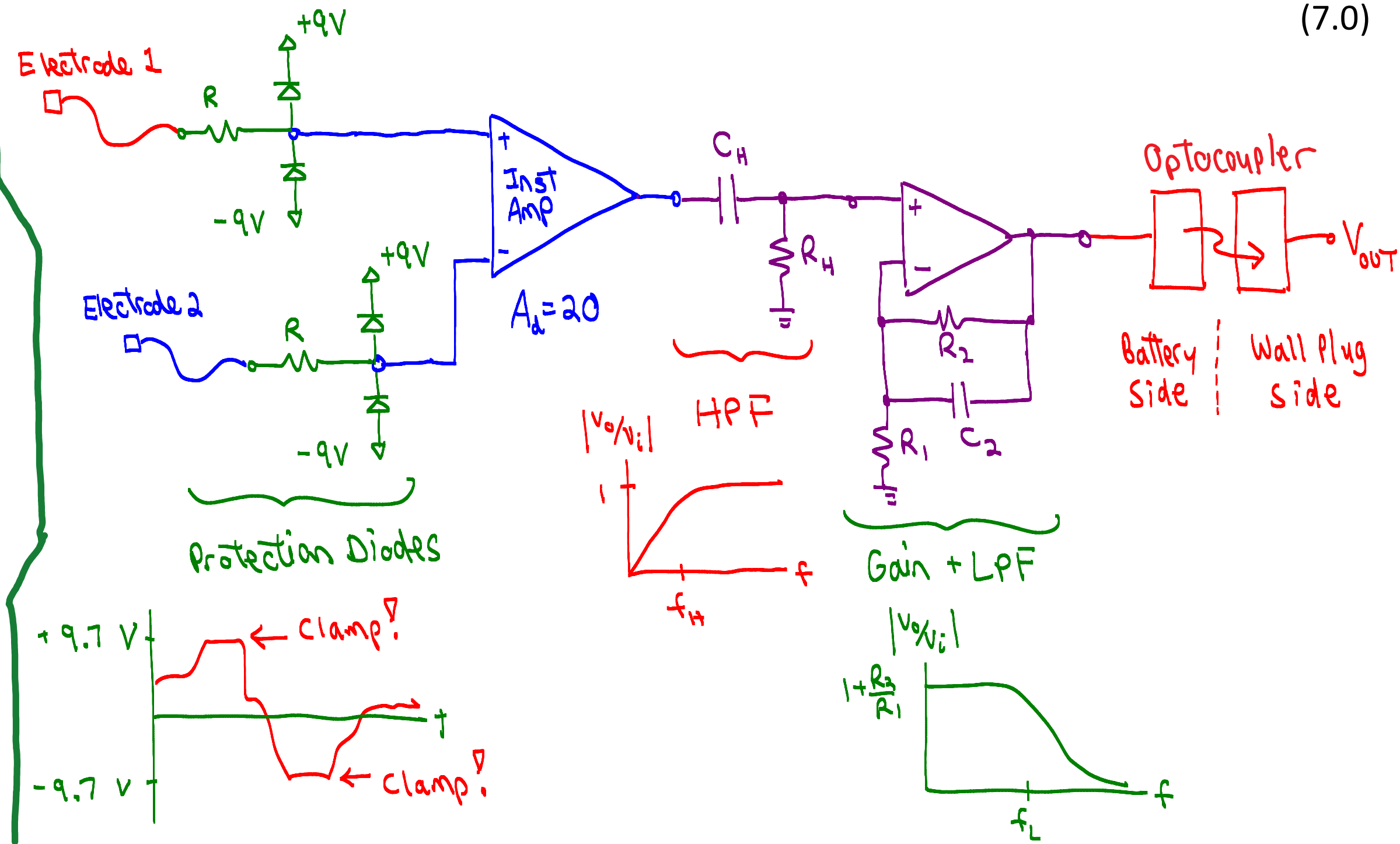
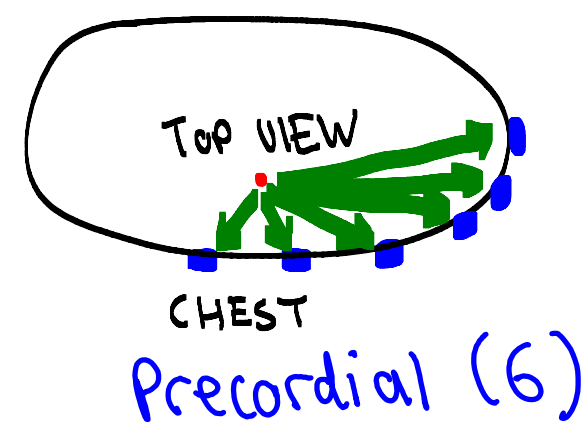
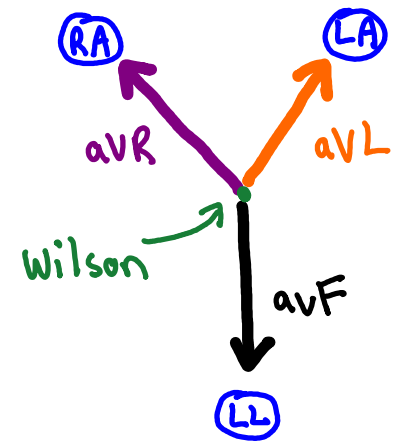
0. Review

12-Lead ECG

(3) Einthoven's Triangle



(3) Augmented



★ Isolation

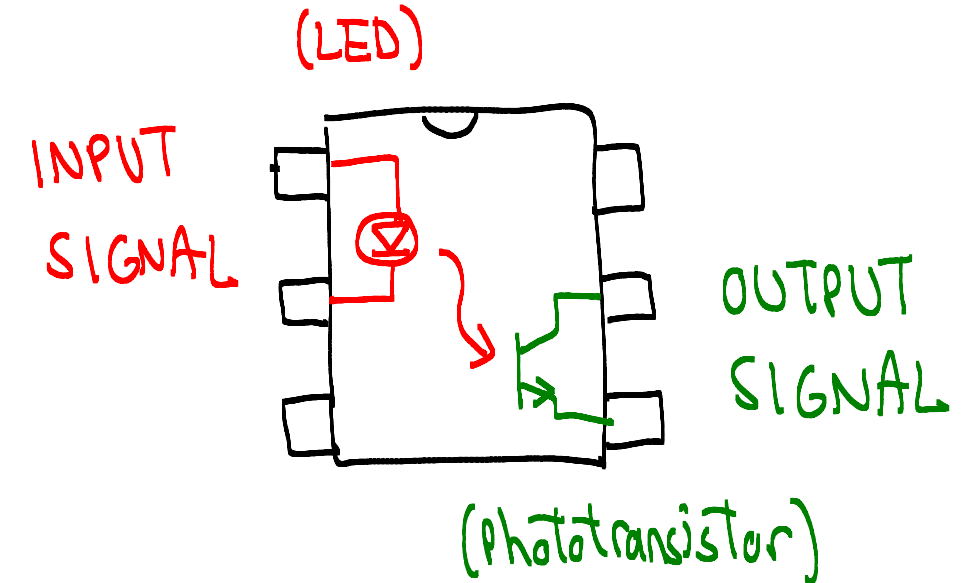
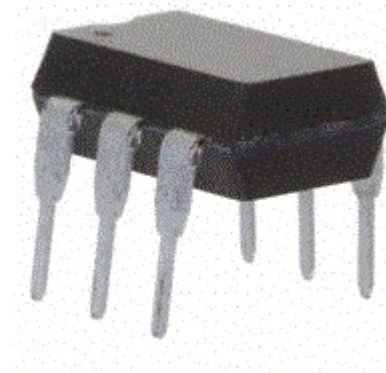
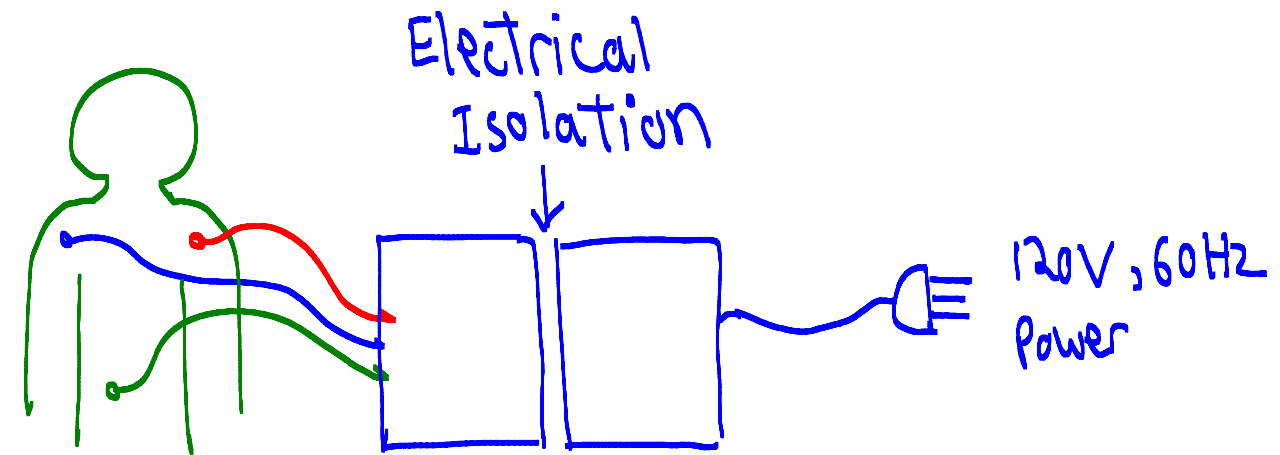
- ECG systems must minimize the possibility of the patient coming in contact with 120V power line

↑ If ECG electronics fail in some manner.

★ An optocoupler (or photocoupler) is a common way to achieve galvanic isolation

↑ no electrical connection

→ Information is transmitted by light, not electricity!



} Commonly used to electrically isolate a circuit from high voltage. (Lots of other applications...)

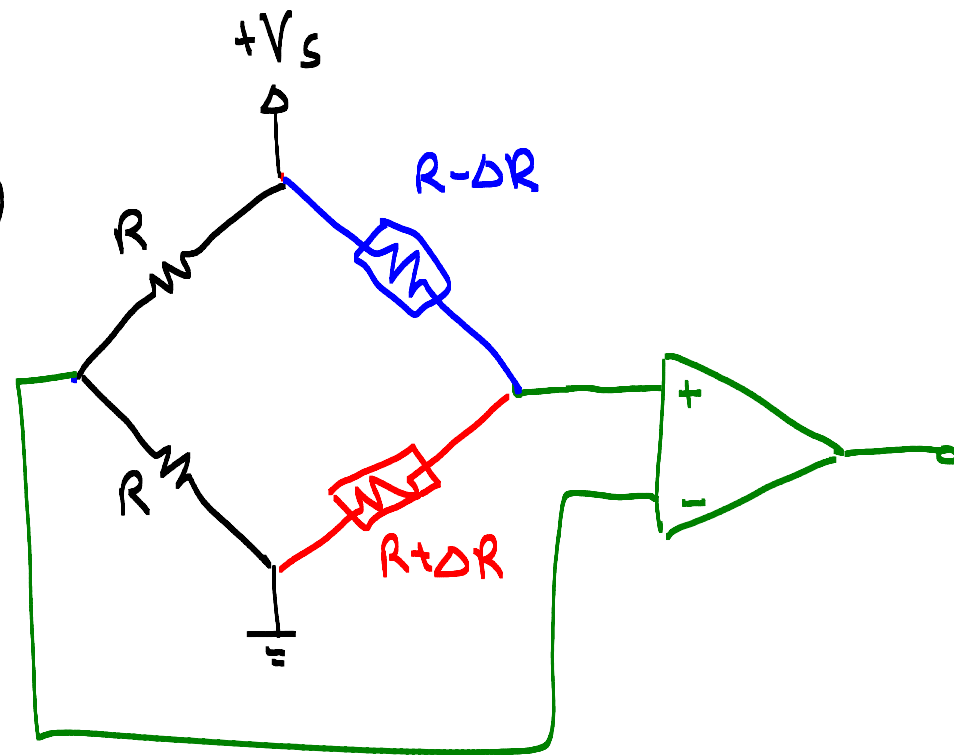
1. Instrumentation Amplifier Basics

A. Differential Amplifier

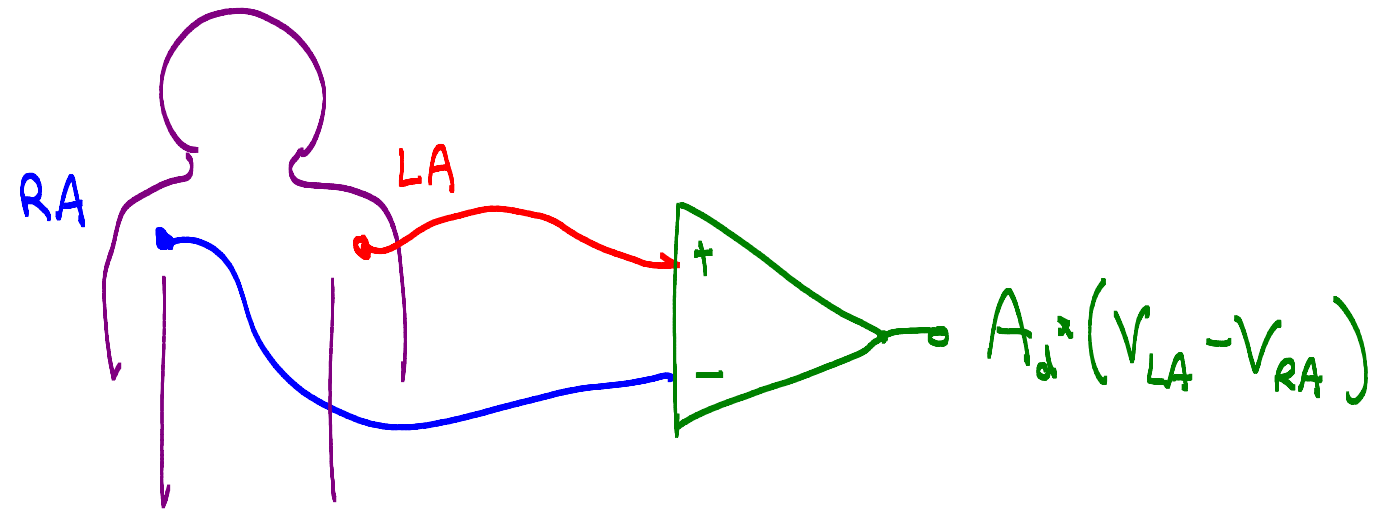
- Many sensors produce a differential output voltage

Ex:

Strain Gage



- In ECG, we want to amplify the voltage between 2 electrodes



$\Rightarrow$ Need a differential amplifier!

B. Single op-Amp Differential Amplifier

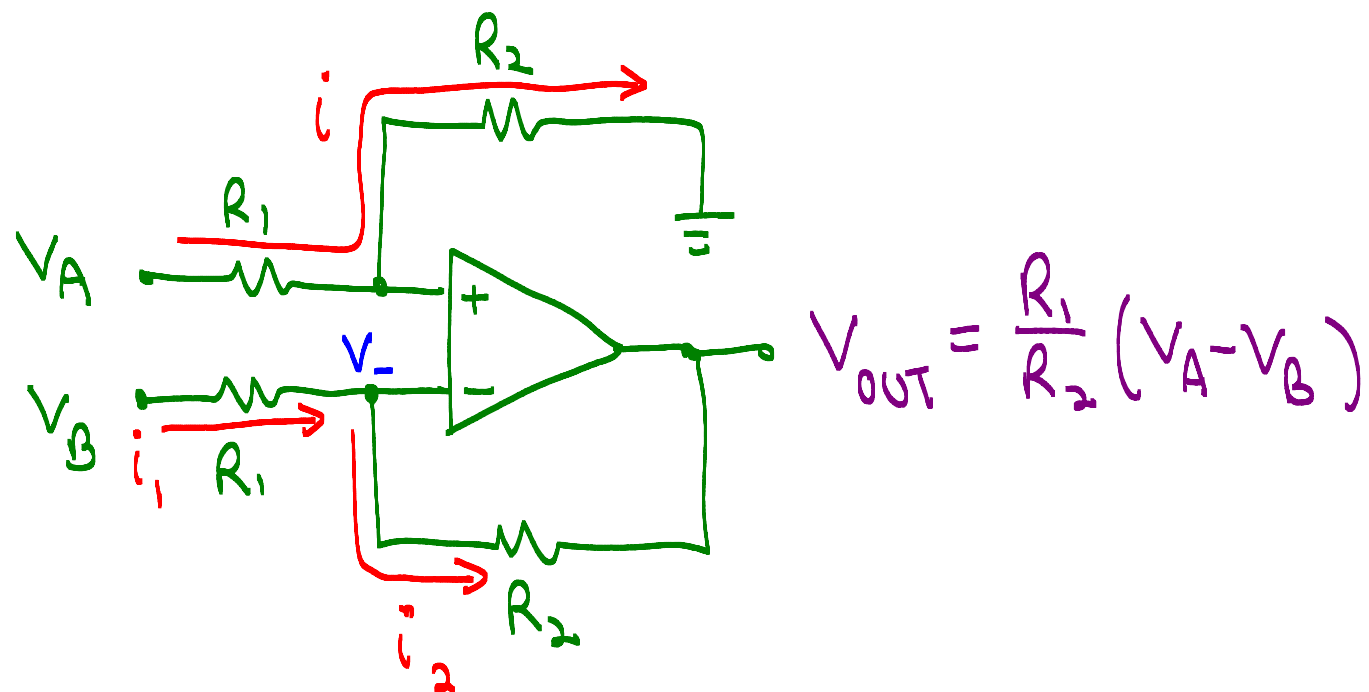
Simplest type of diff amp:

KCL at node V_- :
 $i_1 = i_2 + 0$ ← Golden Rule #2

$$\frac{V_B - V_-}{R_1} = \frac{V_- - V_{OUT}}{R_2}$$

$$\frac{R_2}{R_1} V_B - \left(1 + \frac{R_2}{R_1}\right) V_- = -V_{OUT}$$

$$V_{OUT} = \left(1 + \frac{R_2}{R_1}\right) V_- - \frac{R_2}{R_1} V_B$$



Golden Rule #1: $V_- = V_+ = i R_2 = \frac{V_A}{R_1 + R_2} R_2$

$$\begin{aligned} \Rightarrow V_{OUT} &= \frac{R_1 + R_2}{R_1} \cdot V_A \frac{R_2}{R_1 + R_2} - \frac{R_2}{R_1} V_B \\ &= \frac{R_2}{R_1} (V_A - V_B) \checkmark \end{aligned}$$

- Major drawback of single op amp diff amplifier is modest input impedance (typically $\sim 10\text{K}$).

Who cares?

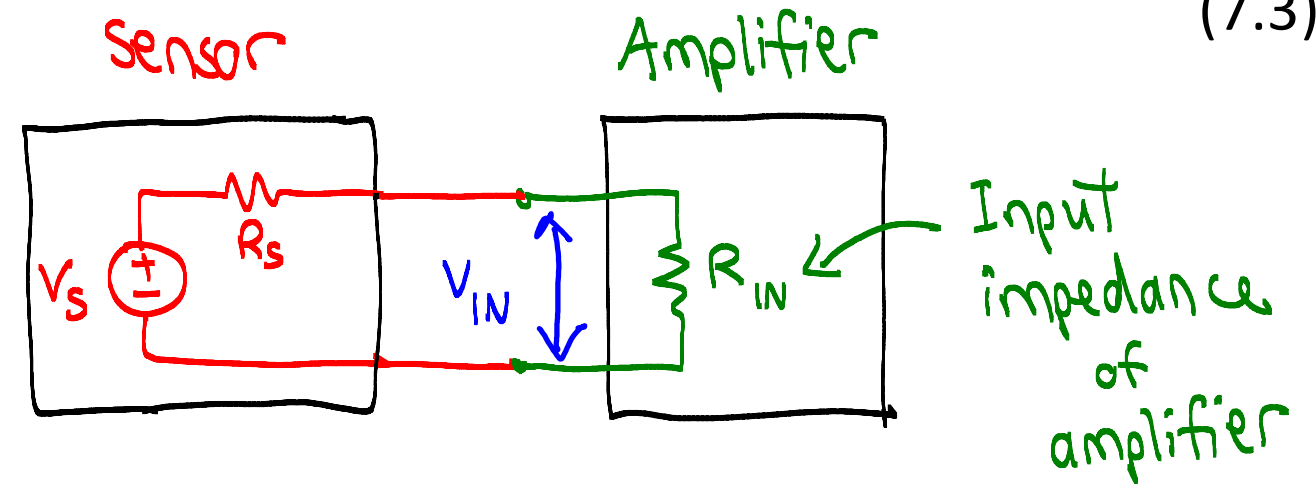
① Sensor can be viewed as a voltage source V_s with output impedance R_s $\leftarrow$ Thevenin!

② Amplifier looks like a resistor R_{in} to the sensor

$\rightarrow R_s$ and R_{in} form a voltage divider!

$\Rightarrow$ Many sensors have $R_s \sim 10\text{K}\Omega$ (even $1\text{M}!$)

$\Rightarrow$ Need large input impedance (e.g. $R_{in} > 100\text{M}$) to minimize signal loss!



$$\star V_{IN} = V_s \frac{R_{in}}{R_{in} + R_s}$$

Ex:

$$V_{IN} = V_s \frac{10\text{K}}{10\text{K} + 10\text{K}} = 0.5V_s \quad \text{☹️}$$

$$V_{IN} = V_s \frac{1\text{M}}{1.01\text{M}} = 0.99V_s \quad \text{😊}$$

Example Thermistor Circuit

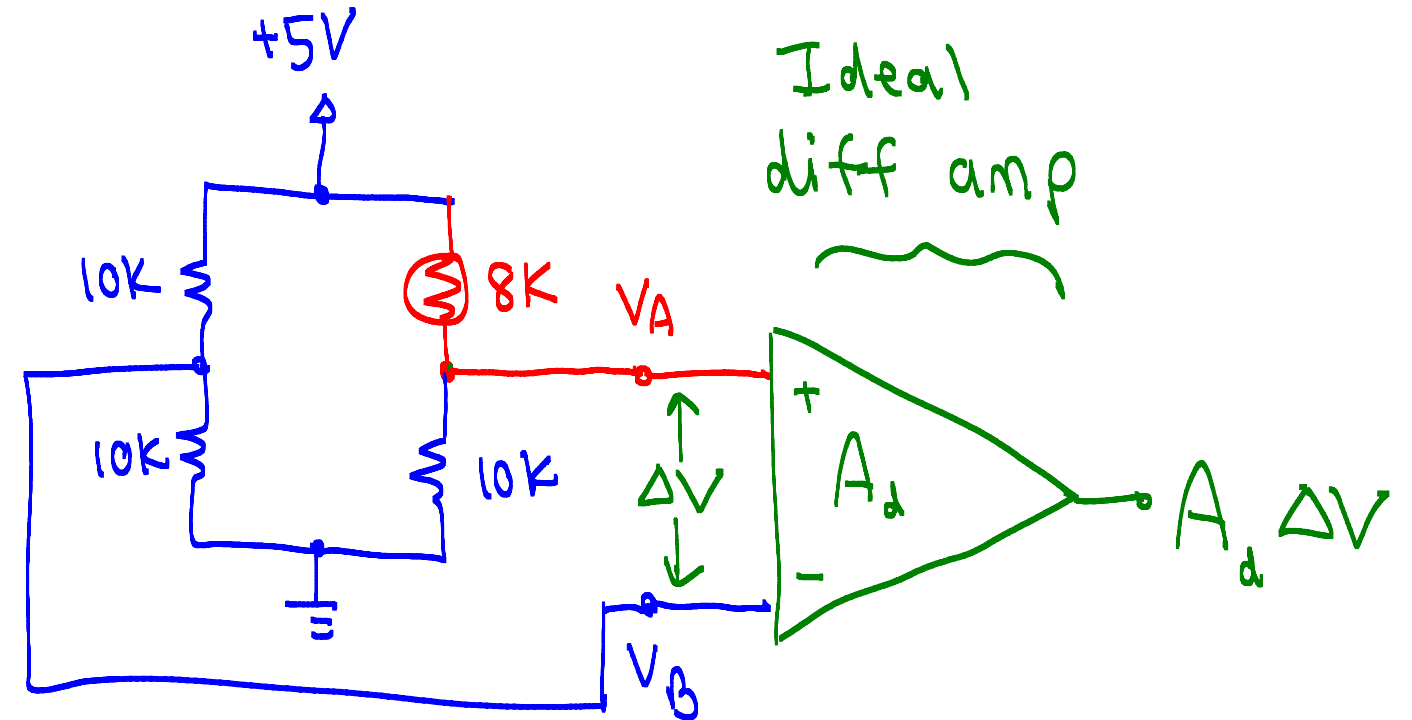
- By itself, the bridge produces

$$V_A = \frac{5V}{8K+10K} \times 10K = 2.78V$$

$$V_B = \frac{5V}{10K+10K} \times 10K = 2.5V$$

$$\rightarrow \Delta V = 2.78 - 2.5 = \boxed{0.28V}$$

- Ideally, a diff amplifier ($A_d = 2$) produces: $A_d \Delta V = 2 \times 0.28 = \boxed{.56V}$



single op amp
diff amplifier
does NOT
produce this!
..

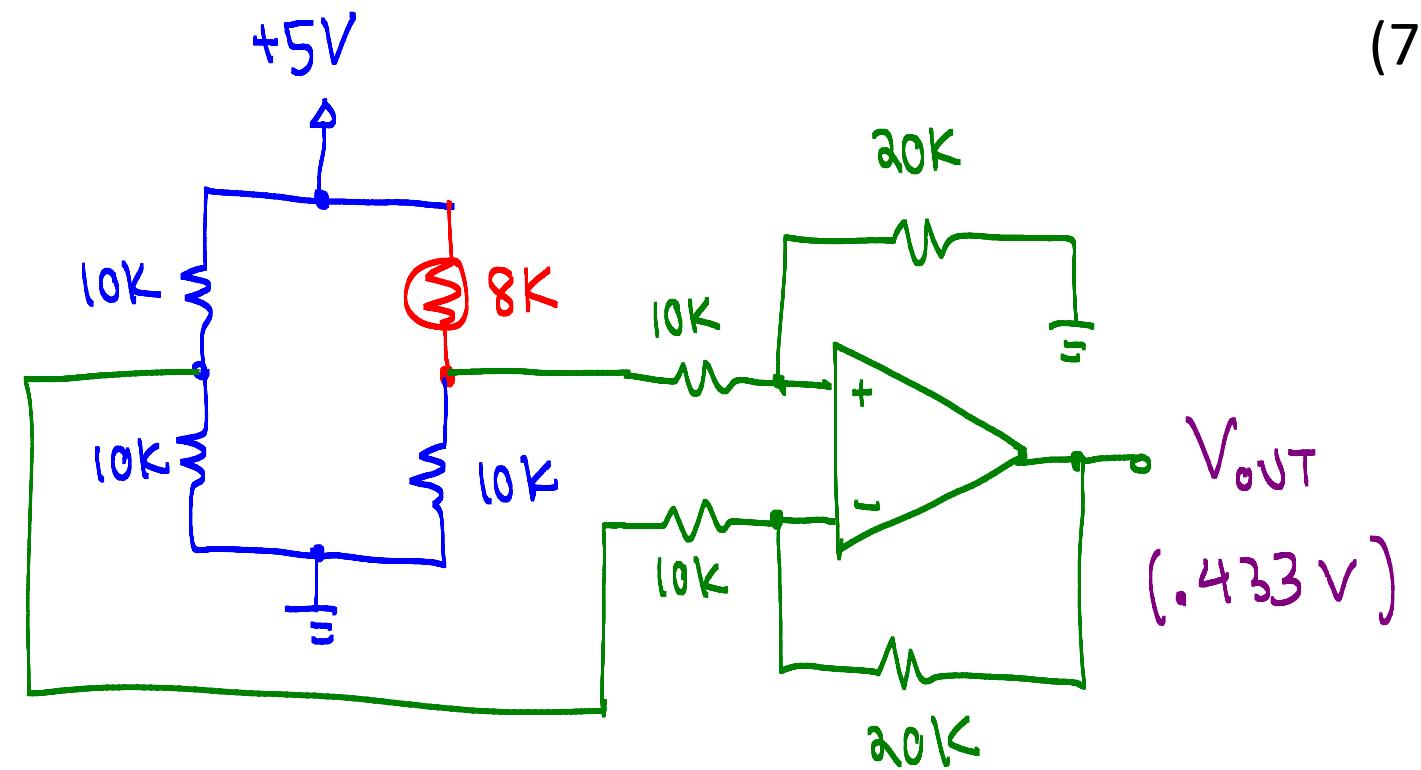
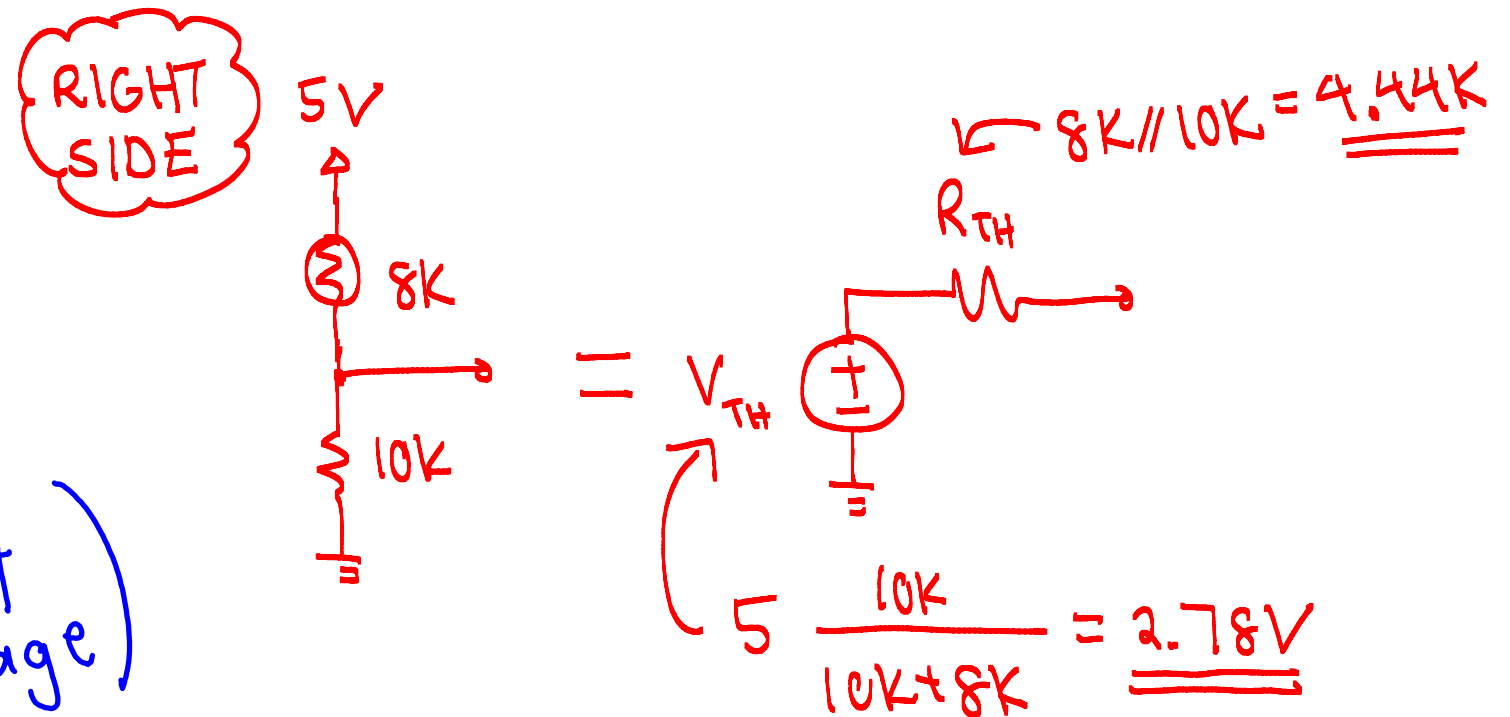
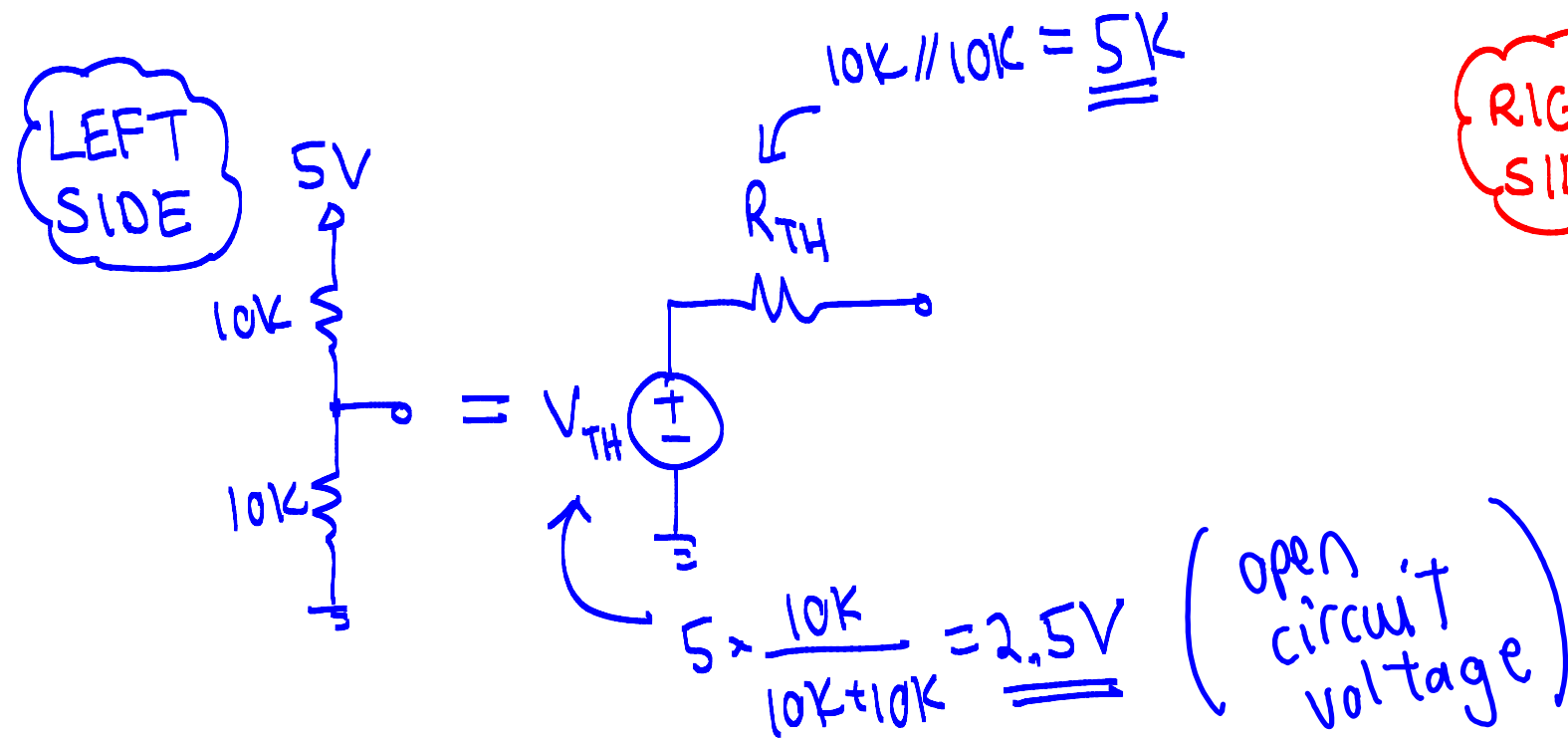
- Now consider using a single op amp diff amplifier.

23 %
error!

Turns out $V_{out} = 0.433V$

Derivation:

① Thevenize the bridge!



② Use Golden Rules
on new circuit:

KCL at node V_- : $i_1 = i_2$

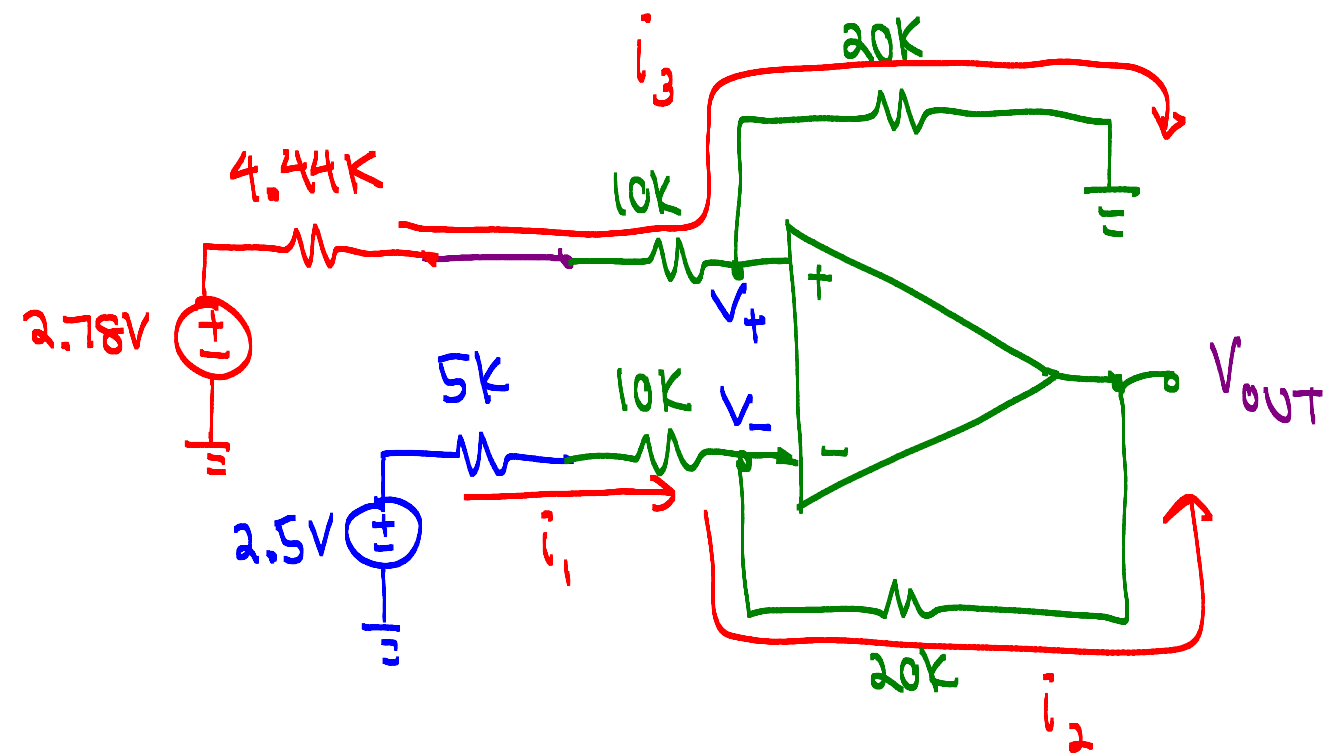
$$\frac{2.5 - V_-}{5K + 10K} = \frac{V_- - V_{OUT}}{20K}$$

$$\Rightarrow V_{OUT} = V_- - 20K \frac{2.5 - V_-}{15K}$$

Rule #1: $V_- = V_+ = i_3 \times 20K$

$$= \frac{2.78 - 0V}{4.44K + 10K + 20K} \times 20K$$

$$= 1.614V$$



$$\Rightarrow V_{OUT} = 1.614 - 20K \cdot \frac{2.5 - 1.614V}{15K}$$

$$= \boxed{0.433V}$$

↑
23% error
(ideal value = 0.56V) ☹

- An instrumentation amplifier is a very high quality diff amplifier

① HUGE input impedance ($\sim G\Omega$)

↳ No signal loss! 😊

② Large common mode rejection ratio (CMRR)

↑?

APPLICATIONS

Weigh scales

ECG and medical instrumentation

Transducer interface

Data acquisition systems

Industrial process controls

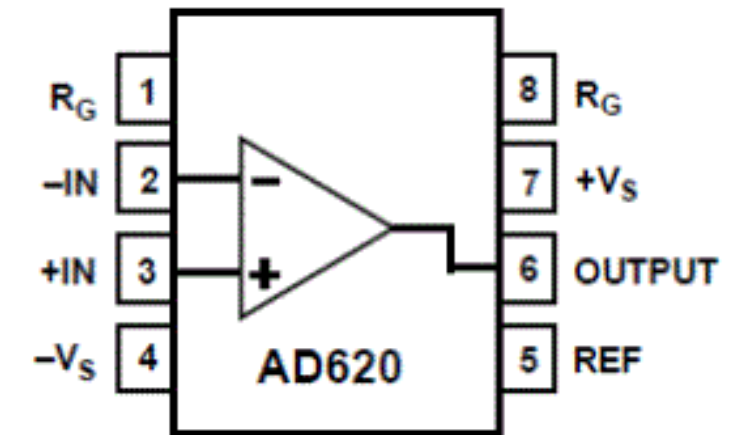
Battery-powered and portable equipment



Low Cost Low Power
Instrumentation Amplifier

AD620

There many other kinds! ↗



2. Common Mode Rejection Ratio (CMRR)

- Ideal output of inst amp:

$$V_{OUT} = V_{REF} + A_d \Delta V$$

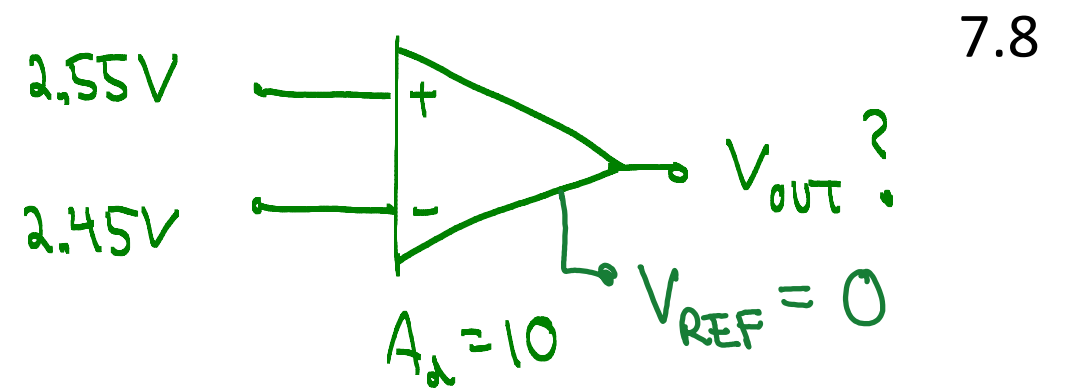
"Differential" Gain $\nearrow$ $\nwarrow$ "Differential input" $V_1 - V_2$

- In reality, an extra "error" term exists!

$$V_{OUT} = V_{REF} + A_d \Delta V + A_{CM} V_{CM}$$

Want this tiny! $\left[\begin{array}{l} \text{"Common Mode Gain"} \\ \text{"Common Mode Input"} \end{array} \right.$ $\nwarrow$ $\nearrow$ $\frac{V_1 + V_2}{2}$

Example



7.8

- Determine inputs: $A_{CM} = 0.01$

(Differential) $\Delta V = 2.55 - 2.45 = 0.1V$

(Common Mode) $V_{CM} = \frac{2.55 + 2.45}{2} = 2.5V$

- Compute V_{OUT} : $\overbrace{A_{CM} V_{CM}}$ error term

$$V_{OUT} = V_{REF} + A_d \Delta V + A_{CM} V_{CM}$$

$$= 0 + \underbrace{10 \times 0.1}_{1.0} + \underbrace{0.01 \times 2.5}_{0.025} = \boxed{1.025V}$$

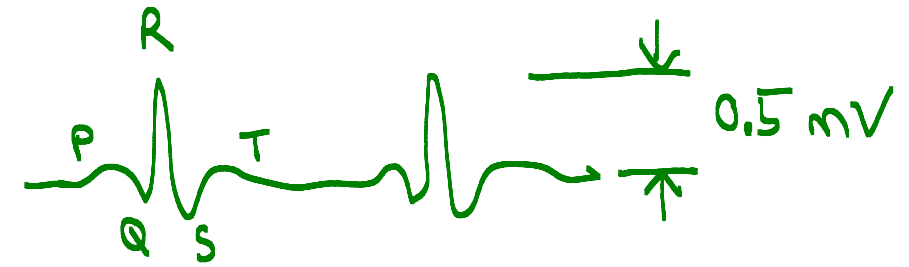
- Common Mode Rejection Ratio (CMRR)

$$\text{CMRR} = 20 \log_{10} \left(\frac{A_d}{A_{cm}} \right)$$

← Good inst amp has CMRR > 100 dB!

$$\frac{A_d}{A_{cm}} = 10^5$$

(7.9)



Example:

ECG input is PQRST waveform with 0.5 mV peak R-wave. Power line interference causes common mode voltage with 1 V_{pp} amplitude.

If $A_d = 30$ and CMRR = 80 dB, what is V_{out} ?

① Inputs: $\Delta V = [0.5 \text{ mV PQRST}]$

$$V_{cm} = 0.5 \sin 2\pi f_o t$$

↖ 60 Hz

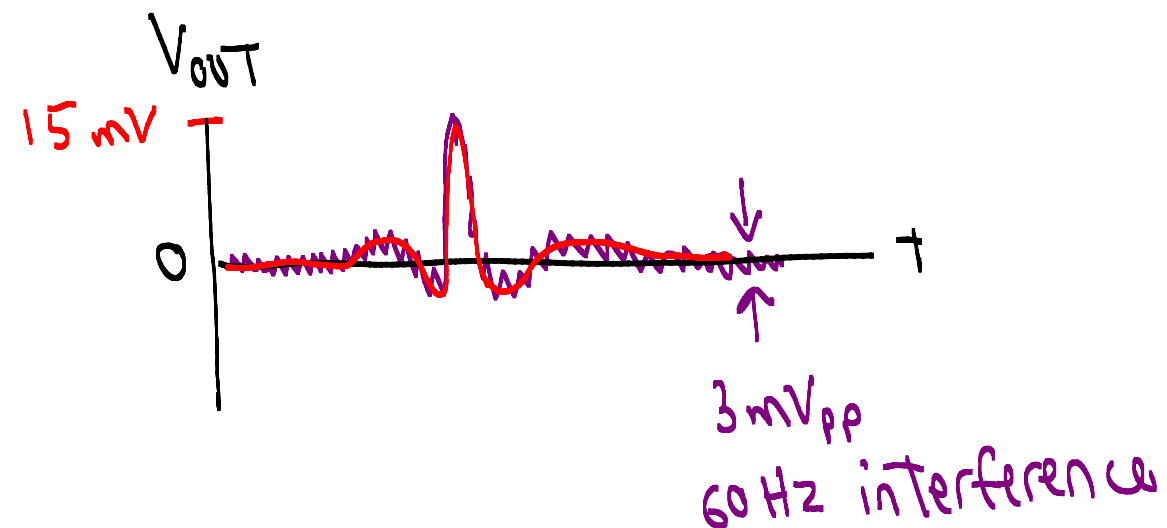
② A_{cm} : $\text{CMRR} = 20 \log_{10} \frac{A_d}{A_{cm}}$

$$\rightarrow \frac{A_d}{A_{cm}} = 10^{\text{CMRR}/20} \Rightarrow A_{cm} = \frac{30}{10^{80/20}} = \underline{\underline{0.003}}$$

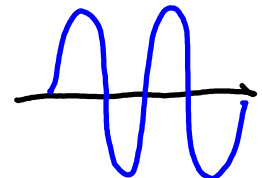
③ output: $V_{out} = A_d \Delta V + A_{cm} V_{cm}$ $\leftarrow$ assume $V_{REF} = 0$
if none given

$$= 30 \times (0.5 \text{ mV PQRS}) + .003 \times 0.5 \sin 2\pi f_o t$$

$$= (15 \text{ mV PQRS}) + \underbrace{.0015 \sin 2\pi f_o t}_{1.5 \text{ mV}} \quad \uparrow 60 \text{ Hz}$$



NOTE:

Peak $\uparrow$  Peak-to-Peak